Following development of the EGR prototype sampling system, field evaluations were performed under USEPA contracts (Williamson, et al., 1985). The Emission Gas Recycle System was used to measure total mass and particulate size fractions at three separate coal-fired power plants. The test series compared results from the EGR system with those from standard Method 17 mass train systems, conventional cyclone and impactor trains, and similar trains using another PM<sub>10</sub> candidate method, SIM5 (Farthing, et al., 1985). During the first two tests, the EGR and conventional cyclone train consisted of Cyclones I and IV of the SoRI/EPA series cyclone train, followed by a 47mm glass fiber filter. For the final test of the series, a full SoRI five-stage series cyclone system was used for both systems. University of Washington Mark V impactors were also used for comparisons in all testing.

#### 5.8.1 TEST NO. 1

The first field test took place at one of the twin 56 MW coal-fired boilers at a utility generating station. The plant nominally operates at minimum (half) load; however, boiler conditions occasionally changed as dictated by demand. The sampling location chosen was the ducting between an outdated, somewhat inefficient electrostatic precipitator and a retro-fitted, more efficient ESP.

The overall test was divided into two subtests. Subtest A involved the comparison of traverses performed with the EGR train and a standard Method 17 (M17) mass train. To eliminate spatial bias, a probe was configured with a cyclone set (SoRI Cyclone I, Cyclone IV and a 47mm filter) using an EGR nozzle and a collocated 47mm filter. The large diameter of this system required plant installation of six-inch ports. Three traverse points were selected which represented the maximum point-to-point velocity change accessible through the six-inch ports. The recycle rate was then adjusted to achieve isokinetic sampling at each point while maintaining the chosen the chosen constant flowrate through the cyclone set. The flowrate through the collocated 47 mm filter was adjusted at each point according to isokinetic sampling protocol.

In Subtest B, the EGR-M17 hardware described under Subtest A was used without modification. A second cyclone train, without emission gas recirculation, was used for a "near-collocated" reference. This train used identical cyclone samplers equipped with a standard nozzle rather than the EGR nozzle. The remainder of the sampling train was conventional: a heated stainless steel probe, ice bath condenser, and a commercial Method 5 control box. Both probes (three sampling trains) were inserted at right angles to each other in order to sample at the same point in the duct (within approximately four-inch nozzle-to-nozzle spacing). The duct point and nozzle for the nonrecycle train which were selected resulted in an isokinetic flowrate that was slightly greater than the flowrate calculated for a  $10\mu m$   $D_{50}$  in the cyclone. The isokinetic flowrate rather than the PM flow rate was used for sampling. The EGR cyclone was fitted with a

smaller nozzle than the nonrecycle train. The EGR sample flowrate was adjusted to maintain isokinetic nozzle sampling. The recycle fraction was adjusted to make the cyclone flowrate identical to that used for the nonrecycle cyclone. The Method 17 sampler was operated in the usual fashion.

A total of eight valid EGR comparison tests were performed during the initial field test. Sampling runs 2 through 6 were completed as described under Subtest A. With the exception of Run 3, which was performed during aperiod of fluctuating boiler load, these were performed with the boiler at full load (56 MW). Runs 7 through 10 were replicates for Subtest B, all of which were run at minimum boiler conditions (28 MW).

The run parameters, along with the total mass and nominal-PM<sub>10</sub> loadings are shown in Table 5-1. The recycle rates (shown as percentage of the total cyclone flowrate) varied from 9.6% to 59.6% during the test series.

## 5.8.2 TEST NO. 2

The second EGR field test was carried out at a 500 MW coal-fired power plant. The plant consisted of two 250 MW units with emission from each unit controlled by two cold-side electrostatic precipitators. The sampling location chosen was between the outlet of one ESP and the stack. Pretest surveys indicated the duct velocity averaged 60 ft/sec, with substantial velocity spread. An aerosol mass median diameter in the 7-14 μm diameter range was expected. As previously mentioned, the cyclone trains used for the second field test were identical to those used for the first test (SoRI Cyclone I, Cyclone IV, and a 47 mm quartz-fiber backup filter). The EGR cyclone train simultaneously sampled a three-point traverse along with a standard sampling cyclone train following another candidate PM, sampling protocol referred to as SIM5 (Synthetic Method 5). The SIM5 protocol was developed to provide valid emissions data for  $10\mu m$  and smaller particles while using a fixed sampling flowrate. The method is not capable of correctly measuring emissions of particles larger than  $10\mu\text{m}$ , consequently no valid total emissions data can be obtained using it.

The flowrates through both trains were set to produce a 10  $\mu m$  aerodynamic D $_{50}$  through the first cyclone. The nonrecycle (SIM5) cyclone train sampled across the traverse at constant flowrate as outlined in the SIM5 protocol. By using a slightly smaller nozzle on the EGR system, the nozzle sampled isokinetically while the total cyclone flowrate was keep constant with the addition of variable amounts of recycle gas. Eight replicates of the paired measurements were initiated. However, equipment malfunctions invalidated the first two EGR runs, and the fifth EGR/SIM5 run was aborted after the boiler dropped from 240 MW to 90 MW due to plugging of a fuel feed line. The run parameters, total mass loadings, and PM $_{10}$  mass loadings for these tests are shown in Table 5-2. As with the first field test, the samples were obtained within 10% of the isokinetic ratio. In this test series the recycle rates consistently averaged around 46%.

Table 5-1. EGR test 1 run parameters.

	Sample Flow (acfm)	Percent Recycle	Percent Isokinetic	Boiler Load (MW)	Mass Loading (mg/dnm <sup>3</sup> )	PM <sub>10</sub> Loading (mg/dnm <sup>3</sup> )
Run 2						
M17	0.67		164.3	56	1557 <sup>a</sup>	
EGR	0.56	18.0	98.1		2053	453
Run 3						
M17	0.57		99.4	34	586	
EGR	0.33	59.6	96.8		543	113
Run 4			•			
M17	0.40		96.1	56	2397	
EGR	0.59	15.6	100.9		1952	391
Run 5						
M17	0.42	-	100.6	56	2077	
EGR	0.62	15.7	107.5		1804	411
Run 6						
M17	0.48		107.7	56	1888	
EGR	0.64	9.6	104.5		1808	399
Run 7						
M17	0.49		104.7	28	61.9	
EGR	0.57	20.8	105.9		42.9	17.8
STD	0.66		89.7		46.5	18.5
Run 8						
M17	0.45		107.2		87.9	
EGR	0.53	41.6	108.8	28	75.7	21.8
STD	0.67		102.7		57.2	21.8
Run 9						
M17	0.49		111.9		65.3	
EGR	0.55	33.6	111.0	28	63.9	20.5
STD	0.74		107.9		67.0	28.8
Run 10						
M17	0.47		99.7		80.9	
EGR	0.56	34.9	101.9	28	74.5	27.8
STD	0.74	<b></b>	100.6		60.4	26.6

<sup>&</sup>lt;sup>a</sup>Ml7 control box malfunction--run deleted from test averages.

Table 5-2. EGR test 2 run parameters.

	Sample Flow (acfm)	Percent Recycle	Percent Isokinetic	Mass Loading (mg/dnm <sup>3</sup> )	PM <sub>10</sub> Loading (mg/dnm <sup>3</sup> )
Run 1					
EGR	0.40	38.9	111.7	a	110
SIM5	0.60		95.1	264	124
Run 2					
EGR	0.33	47.7	98.4	b	
SIM5	0.61		94.0	213	109
Run 3					
EGR	0.34	46.5	96.5	195	94
SIM5	0.62		97.3	201	107
Run 4					
EGR	0.35	46.3	99.7	279	130
SIM5	0.59		92.4	307	138
Run 6					
EGR	0.34	48.6	99.1	115	56
SIM5	0.61		100.2	130	66
Run 7					
EGR	0.34	47.5	99.6	200	86
SIM5	0.60		94.4	207	104
Run 8					
EGR	0.36	45.3	97.1	189	79
SIM5	0.60		91.7	228	104

<sup>&</sup>lt;sup>a</sup>Excessive nozzle scrape -- total mass not included in test averages.

bInvalidated run -- deleted from test averages.

## 5.8.3 TEST NO. 3

The site chosen for the third EGR field test was a 221 MW coal-fired utility boiler. Sampling took place at the inlets to two identical particulate control devices. Eight four-inch ports provided access to the duct interior on each unit. The velocity of Duct A ranged from 37 to 64 ft/sec, with a mean velocity of approximately 51 ft/sec. Duct B had a velocity range of 45 to 61 ft/sec, with an average of 53 ft/sec.

The test plan called for a concurrent EGR/nonrecycle (SIM5) test series similar to that of Test No. 2. The flowrate for each train was chosen such that the aerodynamic  $\textbf{D}_{50}$  for the first cyclone was 10  $\mu \text{m}_{\bullet}$ Across the traverse, the EGR nozzle sampled isokinetically while a constant cyclone flow rate was maintained using a variable fraction of recycle gas. The nonrecycle cyclone train once again sampled according to SIM5 protocol. In this test, full duct (12-point)  $PM_{10}$  measurements were performed rather than the three-point sample in Test 2. Each 12-point traverse involved sampling at three points in four of the eight ports. The eight ports available for sampling on each duct were grouped into two sets of four, ACEG and BDFH. Four sets of simultaneous EGR and nonrecycle (SIM5) runs were performed at the inlet to Unit A. Two traverses were performed in ports ACEG and two in ports BDFH. Two replicates were performed in Duct B using ports ACEG. The sampling hardware used for both the EGR and nonrecycle (SIM5) trains throughout this testing consisted of full SoRI Five-Stage Series Cyclone sets. The run parameters and loadings for the paired cyclone runs are shown in Table 5-3. The recycle rate averaged about 48% with little variation from run to run.

# 5.8.4 RESULTS AND CONCLUSIONS FROM COLLABORATIVE TESTS

Average particulate concentrations and 95% confidence limits from the data obtained in the three test series are summarized in Table 5-4. be seen, the tests covered a broad range of particulate concentrations. every site, the EGR train and the comparison device measured particulate concentrations which agreed within the combined confidence limits of the measurements. Table 5-4 also presents the relative standard deviation (standard deviation expressed as a percentage of the mean value) of each set of runs. In two cases the relative standard deviation of the EGR is over 15% (Site 1 at low load and Site 2). At Site 2 the same degree of variation is seen in measurements with comparison devices. Since the testing coincided with a period of coal pulverizer problems, the variability is easily attributable to source instability. Some indication of source variability was also noted at Site 1 at low load, although the variance of the EGR data is greater than that seen by the other techniques. It is also interesting to note that the precision of the  $PM_{10}$  measurements is better in every case than that of total mass measurements with the same device.

The test plan for all three sites included simultaneous measurements (collocated where possible) with the EGR train and suitable comparison devices in order to minimize the effects of source temporal variability.

Table 5-3. EGR test 3 run parameters.

	Sample Flow (acfm)	Percent Recycle	Percent Isokinetic	Sampling Duct	Mass Loading (mg/dnm <sup>3</sup> )	PM <sub>l0</sub> Loading (mg/dnm <sup>3</sup> )
Run 1						
EGR	0.30	48.4	101.3	A	3630	744
SIM5	0.60		97.2	A	4090	776
Run 2						
EGR	0.31	47.9	100.8	A	3570	791
SIM5	0.58		99.4	A	2920	659
Run 3						
EGR	0.32	44.0	98.9	A	2740	749
SIM5	0.51		105.1	A	3750	650
Run 4						
EGR	0.30	48.4	101.6	A	3810	752
SIM5	0.57		98.5	A	3830	660
Run 5						
EGR	0.31	49.1	99.4	В	3830	814
SIM5	0.56		120.8	В	3270	756
Run 6						
EGR	0.31	52.2	101.1	В	4330	969
SIM5	0.57		105.9	В	3680	794

Table 5-4. Average particulate concentrations observed in EGR test series

			Total	Mass		PM	10
	No. of Runs	L	verage oading g/dnm³)	Relative Standard Deviation (%)	Lo	erage ading /dnm³)	Relative Standard Deviation (%)
Site 1							
High boiler load							
			a				
M17 mass train	3	2120	(±638)	12.1			
EGR cyclone train	4	1904	(±192)	6.3	413	(±44)	6.7
Low boiler load							
M17 mass train	4	74	(±20)	16.8			
EGR cyclone train	4	65	(±24)	23.4	22	(±6.7)	19.1
Std. cyclone train	4	57	(±12)	13.2	23	(±7.5)	19.7
Site 2							
EGR cyclone train	6	196	(±72)	29.7	92	(±26)	7.1
SIM5 cyclone train	7	221	(±51)	24.9		(±23)	6.4
Site 3							
EGR cyclone train	6	3650	(±546)	14.3	803	(±90)	10.7
SIM5 cyclone train	-		(±444)	11.8		(±70)	9.3
	•	5550	\- <del></del> /	11.0	/10	(2/0)	9.3

<sup>95%</sup> confidence intervals are indicated for each mean particulate loading.

Table 5-5 contains a paired run analysis of the test data. The entries in Table 5-5 represent means and 95 percent confidence limits of individual run percentage differences for the paired measurements of total particulate mass or PM<sub>10</sub> concentration. The percentage differences between the EGR and SIM5 values are relative to the mean of the two concentrations. No consistent trend is seen between the EGR and comparison measurements, and the differences typically do not exceed the 95% significance level.

In summary, the EGR train continues to be a promising technique for source particulate measurements. Further development of the technique should include correction of the few design deficiencies discovered during these tests, adaptation of the EGR concept to a cascade impactor for more detailed size distribution measurements, and further field validation of the concept. It is believed that the method has excellent potential to satisfy the requirements of a PM<sub>10</sub> reference method.

Table 5-5. Percentage difference between EGR cyclone train and reference device in paired runs.

	Number of Runs	Total Mass	PM <sub>10</sub>
Site 1 (Method 17)	8	-11.5±8.3	
Site 1 (Nonrecycle cyclone)	4	9.0±28.7	-8.3±27.4
Site 2 (SIM5 cyclone)	5	-9.3±8.4	-15±6.5
Site 3 (SIM5 cyclone)	6	1.6±20.0	11.4±9.7

Quoted values represent the mean and 95 percent confidence limits of the difference between the EGR concentration and the comparison device concentration on individual runs, expressed as a percentage of the overall mean reference concentration.

#### SECTION 6

## FIELD DEMONSTRATION

A field demonstration of the hardware and techniques described in the three protocols was carried out in Sacramento during the week of January 13, 1986. The demonstrations included actual field sampling and explanations of the equipment and techniques in the laboratory.

The number of samples and the extent to which the protocols could be followed in detail were limited by problems in locating a suitable source, and, once a source was decided upon, by problems in the source operation.

Initially, the source to be used for the field demonstration was a petroleum coke fired boiler operated by the Avon Refinery which was located near Concord, CA. The sampling equipment and personnel arrived at that site on the morning of Monday, 1/13 and equipment setup was begun. However, before setup was complete, the sampling ports were found to be restricted in their internal diameters so that the samplers for two of the three methods could not be inserted into the duct. Both the  $PM_{10}$  (EGR) and Five-Stage Cyclone samplers are designed to work through four inch pipe size or larger ports, but four inch ports must be completely unobstructed. The impactors can be inserted through somewhat smaller ports. The sampling ports at the Avon site were four inch pipe nipples, but they contained 1/8 to 3/16 inch weld beads around their inner circumferences and had been mounted off center on four inch holes cut into the ducting. The weld beads and the lips which resulted from the off center mounting of the nipples made insertion of the  ${
m PM}_{1\,0}$  and cyclone samplers impossible. Therefore, the equipment and personnel returned to Sacramento while an alternate site was sought.

On Tuesday, 1/14 a pilot plant gasifier was selected as the field site. The gasifier is operated as a research unit by the State of California at its central steam plant in Sacramento. The material to be gasified is typically wood slash and/or municipal refuse. Emission testing was already underway on the gasifier for other purposes at this time and the methods demonstrations had to be carried out in a way that would not interfere with those tests. The availability of the gasifier for testing was limited by the amount of fuel which was on hand. Sufficient fuel was on hand for only two to three hours of operation, consequently the sampling associated with the methods demonstrations had to take place concurrent with the ongoing emissions tests.

Equipment setup for sampling at the gasifier stack was begun early on 1/14 in preparation for testing on 1/14 and 1/15. Unfortunately, a fan bearing failed on the gasifier, and the day was lost for sampling while repairs were made. Thursday, 1/16 had been reserved for laboratory demonstrations which could not be rescheduled because of conflicts with other activities of the attending personnel. Thus the field sampling was finally limited by fuel availability and other circumstances to two periods of about one hour each on the morning of Wednesday 1/15.

A total of four six-inch ports had been installed on the stack, of which two were free for the demonstration. The four ports were installed in single plane, making simultaneous traverses through all four impossible. Because of

the limited fuel, all sampling for the emission tests and the methods demonstrations had to take place concurrently. The ongoing emissions testing program had priority; therefore the three demonstration systems had to sample through only two ports and do so in a way that would not interfere with the traverses which were being made through the other two. As a consequence, the demonstration runs were made as single point samples in one quadrant of the stack rather than as full traverses as specified by the protocols.

Sampling took place during the first period of gasifier operation with all three of the methods. The two one-hour periods of gasifier operation were separated by too short a period of time to permit the PM<sub>10</sub> sampler to be cleaned up and readied for another run so only one sample was obtained with it. A single run which spanned both periods of gasifier operation was made with the Five-stage Cyclone sampler. The latter is intended to collect material for chemical analysis and a single large sample is more useful for that purpose than two smaller samples. In any case, there would not have been enough time to recover a sample and prepare for a second run in the interval between the two test burns. Two impactor runs were made, one during each period of gasifier operation.

The impactor from the first run was opened and inspected on site at the steam plant shortly after the run was completed to check on stage loadings. These were thought to be too high on the basis of visual inspection and the second run was shortened to one third of the sampling duration used in the first. Even with the reduced sampling time, the catches on three of the stages from the second run were larger than the limits called for in the protocol but they were probably not so large as to invalidate the results.

The collected particulate matter was left in the samplers overnight so that they could be used in the laboratory demonstrations on the 16th. They were then unloaded as part of the lab demonstration. The cyclone samples were recovered by washdowns using methylene chloride as called for by the protocol and preserved for possible chemical analyses so no results can be reported from that run. The demonstration was not to include actual analyses but the samples were saved for possible analysis at a later time at the discretion of the ARB. Results are included here for the two impactor runs and the PM $_{10}$  run. The total concentrations from those three runs were calculated to be 730, 938, and 863 mg/dnm3 for the first and second impactor runs and the PM $_{10}$  run respectively. The concentrations for particles smaller than  $10\,\mu m$  were respectively 568, 797, and 820 mg/dnm3.

Because of the severe overloading in the first impactor run, the results from it should be discounted insofar as the size distribution is concerned. The concentration of particles smaller than  $10\mu m$  from the  $PM_{10}$  sampler is valid (subject to the uncertainty resulting from its being from a single point sample). However, some part of the cyclone catch (particles larger than  $10\mu m$ ) from that run was lost while showing the sample and sampler during the lab demonstration. Therefore the total concentration from the  $PM_{10}$  sample is low by an unknown amount.

The mass median diameter of the emissions as measured in the second impactor run was 2.5 $\mu$ m on an aerodynamic diameter basis and the distribution was approximately log-normal with a sigma-g of about 4. The data suggest that the distribution was really trimodal with the bulk of the emissions in a mode centered at about 2.5 $\mu$ m. The remainder of the emissions would then fall in two lower concentration modes; one centered near 25 $\mu$ m and one near 0.3 $\mu$ m. However, with only one run, and that possibly flawed by overloading, the reality of the latter modes is open to question. Printouts from the PM (EGR) and impactor data reduction programs are given in Figures 6-1, 6-2, and 6-3. These include both the raw data and the final results. Plots of the size distribution results from the second impactor run are given in Figures 6-4 through 6-6.

## EXHAUST GAS RECIRCULATION DATA REDUCTION VERSION 3.3 FEBRUARY 1986

TEST ID. CODE: CARB EGR1

TEST LOCATION: GASSIFIER OUTLET

TEST SITE: SACRAMENTO/CALIFORNIA TEST DATE: 1-15-86 OPERATOR(S): RSMartin

## \*\*\*\* ENTERED RUN DATA \*\*\*\*

TEMPERATURES   T(STK): 310.1 F   T(RCL): 323.4 F   T(LFE): 60.9 F   T(DGM): 56.6 F	SYSTEM PRESSURES DH(ORI): 1.14 INWG DP(TOT): 1.69 INWG P(INL): 5.23 INWG DP(RCL): 1.69 INWG DP(PTO): 0.30 INWG	MISCELLANEA P(BAR): 30.02 INHG DP(STK): 0.00 INMG V(DGM): 10.007 FT3 TIME: 42.00 MIN % CO2: 12.10 % O2: 6.30 NOZ (IN): 0.1853
WATER CONTENT	RAW MASSES	BLANK VALUES
ESTIMATE: 16.9 %	CYCLONE 1: 12.5 MG	CYC RINSE : 0.0 MG
OR	FILTER : 237.4 MG	FILTER HOLDER
CONDENSER: 0.0 ML	TETER 1 ZOTTATIO	RINSE : 0.0 MG
COLUMN : 0.0 GM	IMPINGER	FILTER BLANK : 0.0 MG
000011	RESIDUE: 0.0 MG	IMPINGER
CALIBRATION VALUES	RESIDUE: 8.8 MG	
CP(PITOT) : 0.830		RINSE : 0.0 MG
DH@(ORI) : 10.980		
M(TOT LFE): 0.2298		
B(TOT LFE):0058		
M(RCL LFE): 0.0948		
B(RCL LFE):0007		
DGM GAMMA : 0.9940		

## \*\*\*\*\* REDUCED DATA \*\*\*\*\*

STACK VELOCITY (FT/SEC)	37.11
STACK GAS MOISTURE (%)	16.9
SAMPLE FLOWRATE (ACFM)	0.4263
TOTAL FLOWRATE (ACFM)	0.6687
RECYCLE FLOWRATE (ACFM)	0.2501
PERCENT RECYCLE	36.2
ISOKINETIC RATIO (%)	102.2

	(UM) (PA	(% () RTICULA	(MG/DNCM) ATE)	(GR/ACF)	(GR/DCF)	(LB/DSCF) (X 1E6)
CYCLONE 1 BACKUP FILTER	9.44 	95.0 	43.2 819.6	0.01075 0.20420	0.01882 0.35742	2.69457 51.175
PARTICULATE TOTAL			862.8	0.21495	0.37623	53.870

Figure 6-1. Data and results from the PM10 sampling run during the ARB demonstration.

```
1) PART. DIAMETER
                           CLASSICAL AERODYNAMIC
  2) DATE OF TEST: 1/15/86
  3) TIME OF TEST: 0740
  4) LOCATION OF TEST: GASSIFIER STACK
  5) TEST NUMBER 0
  6) TEST TYPE
                           OUTLET
  7) RUN NUMBER: CARBI-FILE NAME: TORCARB1.OT
 8) RUN REMARKS: OVERLOADED
 10) IMPACTOR TYPE: CARB HIFLO
PC-3-4-5-7-9-11
  9) WATER VAPOR
                           16.90% (KEYBOARD)
     CO2 12.10%
                            CO 1.00%
     02 6.30% N2 80.60%
12) ORIFICE ID (OPTIONAL): .130 NOT IN FILE
13) SUBSTRATE MATERIAL: AP. H ON SS
 1) GAS METER VOL 8.868 CUBIC FEET 2) IMPACTOR DELTA P .00 IN. HG.
 3) ORIFICE DELTA P .00 INCHES H20
4) STACK PRESSURE .00 INCHES H20
 5) BAROMETRIC PRES 30.02 INCHES HG
 6) STACK TEMP 323 DEGREES F
7) METER TEMP 53 DEGREES F
8) IMPACTOR TEMP 323 DEGREES F
9) SAMPLE TIME 20.00 MINUTES
10) AVG GAS VEL 36.14 FEET/SEC
11) ORIFICE PRES
                        .00 INCHES HG
12) NOZZLE DIA .250 INCHES
13) MAX PART DIA 100.0 MICRONS
14) WATER VOLUME
                        .0 CC
15) METER FACTOR
                          1.0148
 MASS GAIN OF STAGE 1 41.15 MG
 MASS GAIN OF STAGE 2 30.06 MG
MASS GAIN OF STAGE 3 34.77 MG
MASS GAIN OF STAGE 4 30.00 MG
 MASS GAIN OF STAGE 5 20.23 MG
 MASS GAIN OF STAGE 6 13.35 MG
 MASS GAIN OF STAGE 7 11.32 MG
 MASS GAIN OF FILTER
                             12.79 MG
MASS GAIN OF BLANK SUBSTRATE
                                          .21
MASS GAIN OF BLANK FILTER
                                          . 14
```

\*\*\*\*\*\*\*\*\*\*\* INPUT DATA \*\*\*\*\*\*\*\*

Figure 6-2a. Data from the first impactor run made during the ARB demonstration.

\*\*\*\*\*\*\*\*\*

TEST NUMBER: 0 RUN NUMBER: CARB1

ACTUAL FLOW RATE .826 CFM
FLOW RATE AT STANDARD CONDITIONS .465 CFM
PERCENT ISOKINETIC 111.810 %

VISCOSITY 219.8E-06GM/CM SEC
CALCULATED IMPACTOR DELTA P = 5.48 IN. HG

STAGE CUNN. DP DP CUM

STAGE	CUNN.	DP	DP	CUM	RE.	VXD50
	CORR.	(CLAS AERO)(	IMP AERO)	FREQ.	NO.	UM-M/S
1	1.025	9.576	9.694	78.684	1410	29.5
2	1.061	3.912	4.029	63.142	612	27.2
3	1.116	2.060	2.176	45.147	252	18.2
4	1.201	1.191	1.305	29.637	320	20.9
5	1.397	.614	.726	19.213	475	23.7
6	1.767	.338	.450	12.371	650	23.6
7	2.461	.196	.307	6.5865	1219	26.5

STAGE CUT DIAMETERS BASED ON THEORETICAL VALUES OF STAGE CONSTANTS
TOTAL MASS CONCENTRATION = 7.30E+02 MG/DRY NORMAL CUBIC METER

SPLINE FIT ON CLASSICAL AERODYNAMIC DIAMETER BASIS

PARTICLE (MICRO			CUM.MASS () (MG/DRY N	DM/DLOGD .CU.METER)
. 100	- 2.0431	2.05	1.50E+01	6.62E+01
.159	- 1.6761	4.69	3.42E+01	1.31E+02
.251	- 1.3401	9.01	6.57E+01	1.79E+02
.398	- 1.0697	14.24	1.04E+02	1.91E+02
.631	8583	19.54	1.43E+02	2.03E+02
1.000	6389	26.15	1.91E+02	3.01E+02
1.585	3281	37.14	2.71E+02	4.92E+02
2.512	.0303	51.21	3.74E+02	5.00E+02
3.981	.3459	63.53	4.64E+02	3.87E+02
6.310	.5982	72.51	5.29E+02	2.78E+02
10.000	.8038	78.93	5.76E+02	9.58E+01
15.850	.9069	81.78	5.97E+02	1.23E+02
25.120	1.1011	86.46	6.31E+02	2.34E+02
39.810	1.6361	94.91	6.92E+02	3.49E+02
63.100	3.7630	99.99	7.30E+02	5.62E+00
100.00	1000000	100.00	7.30E+02	0.00E+00
158.50	1000000	100.00	7.30E+02	0.00E+00
251.20	1000000	100.00	7.30E+02	0.00E+00
398.10	1000000	100.00	7.30E+02	0.00E+00
631.00	1000000	100.00	7.30E+02	0.00E+00

## \*\*\* INHALABLE PARTICULATE MATTER \*\*\*

CUM MASS LESS THAN 1.000 MICRON: 190.76 MG/DNM3 ( 26.15 %) CUM MASS LESS THAN 2.512 MICRON: 373.65 MG/DNM3 ( 51.21 %) CUM MASS LESS THAN 10.000 MICRON: 575.86 MG/DNM3 ( 78.93 %) CUM MASS LESS THAN 15.850 MICRON: 596.68 MG/DNM3 ( 81.78 %) NOTE: DIAMETERS FOR INHALABLE PARTICULATE MATTER ARE ON CLASSICAL AERODYNAMIC BASIS.

Figure 6-2b. Results of the first impactor run made during the ARB demonstration.

```
*********** INPUT DATA ********
 1) PART, DIAMETER
                      CLASSICAL AERODYNAMIC
 2) DATE OF TEST: 1/15/86
 3) TIME OF TEST: 0948
 4) LOCATION OF TEST: GASSIFIER STACK
 5) TEST NUMBER
                  0
 6) TEST TYPE
                     OUTLET
 7) RUN NUMBER: CARB2-FILE NAME: TORCARB2.OT
 8) RUN REMARKS: SHORT RUN
10) IMPACTOR TYPE: CARB HIFLO
PC-3-4-5-7-9-11
 9) WATER VAPOR
                      16.40% (KEYBOARD)
    CO2 12.10%
                      CO 1.00%
        6.30%
                      N2 80.60%
12) ORIFICE ID (OPTIONAL): .130 NOT IN FILE
13) SUBSTRATE MATERIAL: AP. H ON SS
 1) GAS METER VOL
                     3.036 CUBIC FEET
                     .00 IN. HG.
 2) IMPACTOR DELTA P
 3) ORIFICE DELTA P
                     .00 INCHES H20
 4) STACK PRESSURE
                      .00 INCHES H20
 5) BAROMETRIC PRES 30.02 INCHES HG
               310 DEGREES F
 6) STACK TEMP
 7) METER TEMP
                   55
                          DEGREES F
 8) IMPACTOR TEMP 310
                         DEGREES F
 9) SAMPLE TIME
(0) AUG GAS VEL
                    7.00 MINUTES
10) AVG GAS VEL
                   36.14 FEET/SEC
11) ORIFICE PRES
                      .00 INCHES HG
12) NOZZLE DIA
                      .250 INCHES
13)MAX PART DIA
                   100.0 MICRONS
14) WATER VOLUME
                     .0 CC
15) METER FACTOR
                     1.0148
 MASS GAIN OF STAGE 1
                       12.90 MG
 MASS GAIN OF STAGE 2 16.92 MG
 MASS GAIN OF STAGE 3 19.15 MG
MASS GAIN OF STAGE 4
MASS GAIN OF STAGE 5
                       15.71 MG
                       7.76 MG
 MASS GAIN OF STAGE 6
                        5.17 MG
 MASS GAIN OF STAGE 7
                        5.01 MG
MASS GAIN OF FILTER
                        3.60 MG
MASS GAIN OF BLANK SUBSTRATE
                                  .26
MASS GAIN OF BLANK FILTER
                                  .18
```

Figure 6-3a. Data from the second impactor run made during the ARB demonstration.

\*\*\*\*\*\* RESULTS \*\*\*\*\* TEST NUMBER: 0 RUN NUMBER: CARB2 ACTUAL FLOW RATE .787 CFM FLOW RATE AT STANDARD CONDITIONS .453 CFM PERCENT ISOKINETIC 106.493 % VISCOSITY 217.2E-06GM/CM SEC CALCULATED IMPACTOR DELTA P = 5.02 IN. HG STAGE CUNN. DΡ DP CUM RE. VXD50 CORR. (CLAS AERO) (IMP AERO) FREQ. NO. UM-M/S 1.024 9.760 9.876 84.992 1384 28.6 1.059 3.990 4.105 65.210 601 26.5 3 1.111 2.107 2.221 42.781 247 17.8 1.191 4 1.222 1.334 24.436 315 20.4 1.377 .633 .742 15.531 466 23.2 1.720 9.7008 .459 .350 638 23.2 2.354 .205 .314 4.0608 1197 26.3 STAGE CUT DIAMETERS BASED ON THEORETICAL VALUES OF STAGE CONSTANTS TOTAL MASS CONCENTRATION = 9.38E+02 MG/DRY NORMAL CUBIC METER SPLINE FIT ON CLASSICAL AERODYNAMIC DIAMETER BASIS PARTICLE DIA. CUMFR CUMFR CUM.MASS DM/DL0GD (MICRONS) (STDDEV) (PERCENT) (MG/DRY N.CU.METER) .100 - 2.5728 4.74E+00 .51 3.65E+01 2.07 1.94E+01 1.25E+02 .159 - 2.0394 .251 - 1.5598 5.94 5.57E+01 2.23E+02 .3887 .7351 3.981 65.12 6.11E+02 6.44E+02 76.89 7.21E+02 4.67E+02 6.310 10.000 1.0476 85.26 8.00E+02 2.35E+02 15.850 1.2766 89.91 8.44E+02 2.09E+02 25.120 1.5947 94.46 8.86E+02 2.19E+02 39.810 2.2519 98.78 9.27E+02 1.53E+02 39.810 4.4991 100.00 9.38E+02 3.55E-01 63.100 100.00 1000000 100.00 9.38E+02 0.00E+00 158.50 1000000 100.00 9.38E+02 0.00E+00 251.20 1000000 100.00 9.38E+02 0.00E+00 398.10 1000000 100.00 9.38E+02 0.00E+00 631.00 1000000 100.00 9.38E+02 0.00E+00 \*\*\* INHALABLE PARTICULATE MATTER \*\*\* CUM MASS LESS THAN 1.000 MICRON: 193.49 MG/DNM3 ( 20.62 %) CUM MASS LESS THAN 2.512 MICRON: 464.48 MG/DNM3 ( 49.51 %)

Figure 6-3b. Results of the second impactor run made during the ARB demonstration.

CUM MASS LESS THAN 10.000 MICRON: 799.89 MG/DNM3 ( 85.26 %) CUM MASS LESS THAN 15.850 MICRON: 843.56 MG/DNM3 ( 89.91 %)

NOTE: DIAMETERS FOR INHALABLE PARTICULATE MATTER ARE

ON CLASSICAL AERODYNAMIC BASIS.

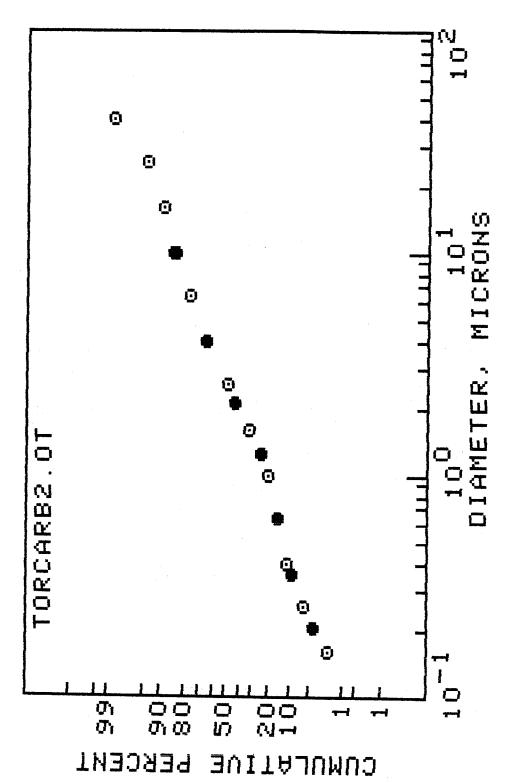


Figure 6-4. Particle size distribution results on a cumulative percentage basis as obtained from the second impactor run of the demonstration testing.

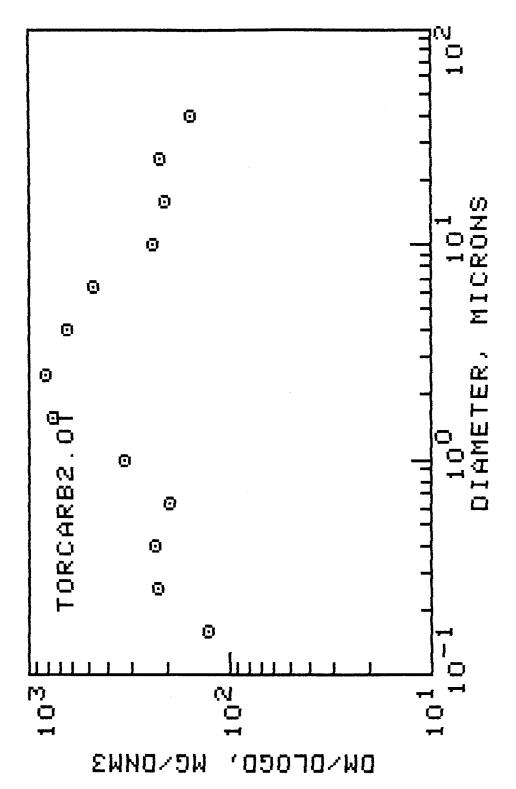


Figure 6-5. Particle size distribution results on a differential mass concentration basis as obtained from the second impactor run of the demonstration testing.

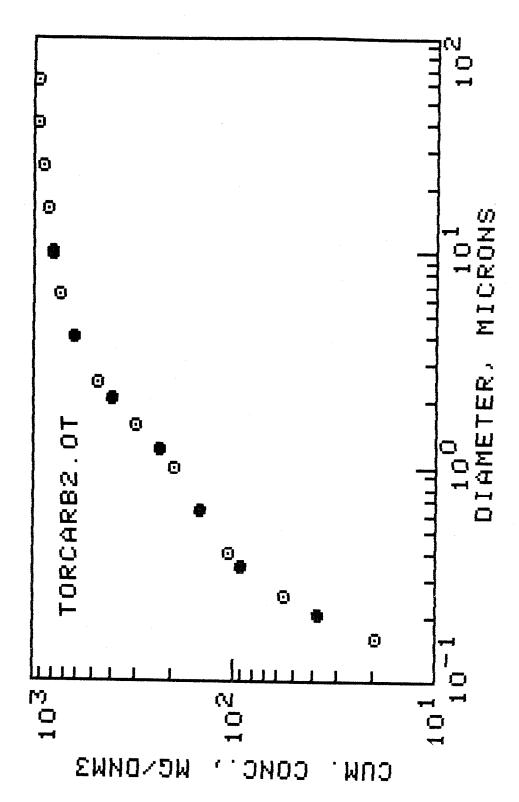


Figure 6-6. Particle size distribution results on a cumulative mass concentration basis from the second impactor run of the demonstration testing.

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### APPENDIX

This Appendix provides a summary of the information gathered in the literature survey described in Section 2 of the report. The presentation format we have used was chosen because it facilitates comparison between the various instruments. The first table defines abbreviations used in the remaining tables and the second gives address information for the different manufacturers. Table A-3 presents equipment arranged alphabetically by manufacturer, while Table A-4 is sorted by "instrument type" code (sampling method). All the information given in Table A-3 is also contained in Table A-4 but is sorted differently. The last two tables are also sorted by sampling method and provide additional information on each of the instruments. For clarity, each instrument has been given a unique "Key Number" which appears in the first column of each table. Paragraphs in Section 2 of the report discuss the various sampling and measurement methods used in the tables.

Each instrument has been identified by a code (use code) which indicates how it may be used to characterize an industrial source. These six usage codes are as follows: FG:I for Flue Gas: In-situ operation; FG:E for Flue Gas: Extractive Techniques; AAA for Ambient Airborne Aerosol monitor, used in conjunction with a sample extraction/dilution system (DIL); L:AR for off-line (laboratory only) techniques involving airborne redispersion of the particulate from a bulk sample; L:LS for off-line techniques involving suspension of the particulate in a nonsoluble liquid; and L:Oth for off-line techniques other than those covered by airborne redispersion or suspension in a liquid. An additional code MA, is used to identify "Major Accessory" items used in conjunction with a The use code of most significance to the reader will given sizing method. probably be "FG:I" (Flue Gas: In-situ). The other codes identify instrumentation which can provide some information but are generally inadequate by themselves to characterize a source. The pricing information listed herein is for general information only. The exact price is set by the vendor and depends on the options selected. The pricing information shown was obtained by telephone in April 1985. The information is presented in the following six tables:

Table A-1: Nomenclature

Table A-2: Manufacturer's Address List

Table A-3: Manufacturer's Model Numbers

Table A-4: Instrument Type Sorted: Description

Table A-5: Instrument Type Sorted: More Description

Table A-6: Instrument Type Sorted: Specifications

Table A-1 Page 1 of 2

#### Comments

Use Codes (Measurement Environment for the Instrument): FG:I Flue Gas: Insitu operation

FG:E Flue Gas: Extractive Techniques used

AAA Ambient Airborn Aerosol monitor (useful with Dilution)

L:AR Laboratory only: Airborn Redispersion from Bulk Powder

L:LS Laboratory Only: Liquid Suspension of the particulate

L:Oth Laboratory Only: Other technique, Image Analysis, etc.

MA Major Accesory to a Primary Sizing Inst. (Data An., etc)

## Inst. Type: Codes Used:

AT Aerodynamic Transport (Laser Doppler Velocity technique for sizing)

AV Alternate Vender; see primary vender for data specifics.

CET Centrifugal Seperation (Bahco and Spiral Centrifuge)

CNC Condensation Nucli Counter (No sizing, conc. only )

CSED Centrifugal Sedimentation

CYC Cyclone sizing systems (centrifugal seperation)

DB Diffusion Battery, screen, tube, plate, etc. (needs a second inst. to measure concentration )

GSED Gravitational Sedimentation

I:A Impactor accesories ( Percollectors, etc. )

IAN Image Analysis System (from photo micrograph or Video of SEM or TEM w/wo EDX for elemental chemistry by size

MA Major accesory to the sizing instrument, data reductionpulse heighth analysis, etc.

MT17 Method 17 Mass Train ( no oven, in-situ ), for use in running Impactors or Cyclones

Misc Miscellaneous sizing techniques not included by the other Misc codes

O:A (OPC) Optical Particle Counter, for Aerosols (airborn), time averaged light scattering, scattered intensity

O:FD Optical: Fraunhofer Diffraction pattern analysis, light scattering, spatical distribution

O:L (OPC) Optical Particle Counter, for liquid suspensions, time averaged light scattering, scattered intensity

O:LB Optical: Light blockage

O:PC Optical: Photon Correlation Spectroscopy (time dependent light scattering based on Brownian Motion)

PHA Pulse Heighth Analysis Inst. MCA's, DAS (Data Aquisition Systems-printed, magnetic tape, BCD for Micros, etc.)

RP Resistivity Pulse (Electrical sensing zone, Coulter

## Comments

Principle

SIV Screen Sieving (manual and automated)

ZZZ Manufacturer's Name, code used to sort Mfg. to bottom.

Other Abbreviations Used In Text:

ch channel

CRM Clean Room Monitoring Inst, off the shelf

CRT Cathode Ray Tube, ie. Computer Monitor or for Oscilloscope

DNA Data NOT available from product literature.

DR Data Reduction / Data Analysis

EDS Energy Dispersive Spectromerty

Fr Fraction, the number of size fractions the instrument gives data on (includes the filter).

Imp Impactor

LAS Laser Aerosol Spectrometer

LPC Laser Particle Counter

Table A-2 PAGE: 1 of 3

### MANUFACTURER'S ADDRESS LIST

\_\_\_\_\_\_\_ COMPANY NAME (DIV OF) Brookhaven Instruments Corp. PARENT COMPANY Equipark Industrial Complex P.O. BOX 200 Thirteenth Ave. STREET ADDRESS Ronkonkoma, NY 11779 (ZIP) California Measurements, Inc. Accurex Div of 150 E. Montecito Ave. Andersen Group Sierra Madre, CA 91024 4215 Wendell Drive Atlanta, GA 30336 Canberra Industries, Inc. One State Street Air Pollution Technology Inc. Meriden, CT 06450 5191 Santa Fe St. San Diego, CA 92109 Climet Instruments Co. Div. of Wehr Corp. Andersen Samplers Div. of P.O. Box 151 Andersen Group 1320 W. Colton Ave. 4215 Wendell Drive Redlands, CA 92373 Atlanta, GA 30336 Coulter Electronics, Inc. Artek Systems Corp. P.O. Box 2145 Farmingdale, NY 590 West Twentieth St. Hialeah, FL 33012-0145 ATM Corporation Sonic Sifter Division Coulter Electronics Inc. 645 S. 94th Place 2140 New Market Parkway, Suite 120 West Allis, WI 53214 Marietta, GA Bausch & Lomb ETC (Energy Technology Consultants) Analytical Products Div, Dpt. 8224 4758 Old William Penn Highway 820 Linden Ave Murrysville, PA 15668 Rochester, NY 14625 Environment One Corp. Belfort Instrument Co. 2773 Balltown Rd. Subsidiary of TransTechnology Corp. Schenectady, NY 12309 727 South Wolfe Street Baltimore, MD 21231 Faley International Corp. P.O. Box 669 Berkeley Controls Inc. EL Toro, CA 92630 Div. of Telonic Berkeley Inc. P.O. Box 277 Fisher Foundery, George, Inc. 2825 Laguna Canyon Rd. 407 Hodley St. 92652 Laguna Beach, CA Holly, Michigan 48442

# MANUFACTURER'S ADDRESS LIST

Flow Sensor Div. of		Leeds & Northrup Co.	
Anderson Group		Unit of General Signal	
4215 Wendell Drive		Microtrac Div.	
Atlanta, GA	30336	3000 Old Roosevelt Blvd.	
•		St. Petersburg, FL	22702
General Electric		oc. receisburg, ru	33702
Ordnance Systems		LeMont Scientific, Inc.	
#1 River Rd., Bldg. 85-16B		2011 Pine Hall Drive, Science	D1-
Schenectady, NY	12345	State College, PA	16801
	12343	bcate correge, FA	1 080 1
Gilson Company, Inc		Malvern Instrumen s Inc.	
P.O. Box 677		187 Oaks Road	
Worthington, OH	43085	Framingham, MA	01701
3 . , .	.000	rramriigham, MA	01701
Hiac/Royco		Marco Scientific, Inc.	
Instruments Div.		1055 Sunnyvale-Saratoga Rd.	40
141 Jefferson Dr.		Sunnyvale, CA	
Menlo Park, CA	94025	Sumyvare, CA	94087
	31023		
Horiba Instruments, Inc.		Micromeritics Instrument Con	en.
1021 Duryea Ave.		5680 Goshen Springs Road	rp.
Irvine, CA		Norcross, GA	30093
·		Hololoss, GA	30093
In Tox		Nikon	
1712 Virginia N.E.			
Albuquerque, NM	87110		
J.B. Systems		Munhall Co., The	
P.O. Box 2405		5655 N. High St.	
La Grange, GA	30241	Worthington, OH	43085
		<b>3</b>	10000
Joyce-Loebl Div. of		Nuclear Data Inc.	
Vickers Instruments Inc.		Golf and Meacham Roads	
Riverview Business Park No.	27	Schaumburg, IL	60196
P.O. Box 99		3,	00.50
300 Commercial St.		Nutech Corp.	
Malden, MA	02148	2806 Cheek Road	
		Durham, NC	27704
Kanomax International Corp.		•	2,,,,,
2-1, Shimizu, Suita		Optomax Inc.	
Osaka, Japan		9 Ash St., Rt. 130	
		Hollis, NH	03049
Leeds & Northrup Co.		,	03043
Unit of General Signal			
Research Division			
Dickerson Road			
North Wales, PA	19454		
	_		

Table A-2 PAGE: 3 of 3

### MANUFACTURER'S ADDRESS LIST

Particle Data, Inc. Varian Inc. Vaarian Palo Alto Vacuum Div. Box 265 (111 Hahn) 60126 Elmhurst, IL Palo Alto, CA 94303 Particle Measuring Systems Inc. Wyatt Technology 1855 South 57th Court P.O. Box 3003 80301 93130 Boulder, CO Santa Barbara, CA Pollution Control Systems Corp. Zeiss 4530 Union Bay Place N.E. One Zeiss Drive 98105 Thornwood, NY 10594 Seattle, Washington Polytec Optronics, Inc. Zoltek Corporation 22651 Lambart St. Unit 108 3101 McKelvey Rd. 63044 El Toro, CA 92630 St Louis, MO Research Appliance Co. Div. of Andersen Group 4215 Wendell Drive Atlanta, GA 30336 Sierra Instruments Div. of Andersen Group 4215 Wendell Drive 30336 Atlanta, GA SDL (Spectron Development Laboratories) 3303 Harbor Blvd., Suite G-3 Costa Mesa, CA 92626 Spectrex Corp. 3594 Haven Ave. 94063 Redwood City, CA Sandia National Laboratories 94550 Livermore, CA TSI Incorporated P.O. BOX 43394 55164 St Paul, MN Unitron, Inc. 175 Express St.

11803

Plainview, NY

CODES, column headings, etc is found in Cyclone Set, Extractive, High Flowrate Special Purpose Impactor, High Temp&Fres #50-800 High Grain Loading Imp., Inlet, gm/stage #50-160 Any, see Flow Sensor #55-690 Anb. Low Pressure Impactor Frecollector Amb. Low Pressure Impactors, etc. Mass Train, for running Impactors, etc. Mass Train, for running Impactors, etc. Image Analysis Automated screen sieving, 5 screens Image Analysis SEM/EDS Interface, Elem. Chem. by size Amb. Impactor, Quartz Crystal Microbal. OPC (P Cor.), liquidborn Amb. Impactor, Quartz Crystal Microbal. Amb. Impactor, Quartz Crystal Microbal. OPC (P Cor.), liquidborn Amb. Impactor, Airborn, Req. 8040 OPC cor., Mass Ach, Data R. & print Optical Part. Ct., Airborn, CleanRoomMont Volume Displacement of Electrolyte Data Analysis for Ta/II L/3 Coul. ctr. OPC (P Cor.), liquidborn  test lab: chem. by size & Morph.; SEM Pulsed Flow Condensation Nuclei Counter Diffusion Battery, Tubular Optical Part. Ct., Airborn, CleanRoomMont Optical Part. Ct., Airborn, CleanRoomMont Optical Part. Ct., Airborn, CRAM, 1 ACFM Optical Part. Ct., Airborn, CLAM, 1 ACFM Optical Part. Ct., Airborn, CLAM, 1 ACFM Optical Part. Ct., Airborn, CLAM, 1 ACFM Optical Part. Ct., Airborn, CRAM, 1 ACFM Optical Part. Ct., Airborn		Key Parameters	Type Code	e Use e Code	Quote x 1000
Special Special Multi High G AV, se Inline Amb. I Mass T Mab. I Amb. I A	etc is found in H	HELP-VENDERS, DAT	222	222	
Species Multi High G AV, se Inline AMD, In Mass T M	High Flowrate	4 Fr(F,1->10 ), complete train; acc.	OgM.	ZZZ FG:E	26.5
Multi High G AV, se Inline Amb. I Amb. I Amb	Temp&Pres	7 Fr(F,.18->25 ),1000F, 10Atm	ZZZ I:CI	ZZZ [ FG:I	7.0
Multi High G AV, se Inline Amb. I Amb. I Amb			222		
High Grain Loading Imp., Inlet, AV, see Flow Sensor #55-690 Inline Amb. Low Pressure Impactor Mass Train, for running Impacto Mass Train, for running Impactor Image Analysis Automated screen sieving, 5 scre Image Analysis SEM/EDS Interface, Elem. Chem. Amb. Impactor, Quartz Crystal M Amb. Impactor, Quartz Crystal M Amb. Impactor, Quartz Crystal M Amb. Impactor, Airborn, Req OPC (P Cor.), liquidborn  OPC (P Cor.), liquidborn  Amb. Impactor, Airborn, Cleani OPC acc., MCA 24Ch, Data R. o OPC acc., MCA 24Ch, Data R. o OPT cac., MCA 24Ch, Data R. o OPT cac., Inquidborn  test lab: chem. by size & Morg Pulsed Flow Condensation Nuclei Diffusion Battery, Tubular Optical Part. Ct., Airborn, Cleani Printer ploter acc. for Faley	Stk Smp	9 Fr(F, 0.4-> 10)	I:CI	FG:I	4.2
Any, see Flow S Inline Amb. Low Presss Mass Train, for Mass Train, for Image Analysis Automated scree Image Analysis SEM/EDS Interfs Amb. Impactor, OPC (P Cor.), Amb. Impactor, OPC (P Cor.), Amb. Impactor, Amb. Impactor, Amb. Impactor, Amb. Impactor, OPC (P Cor.), Independent of the Correspondent of th	gm/stage	4 Fr(F,1.5-> 11), several grams			5.9
Amb. Low Press Mass Train, for Mass Train, for Mass Train, for Mass Train, for Image Analysis SEM/EDS Interfit Amb. Impactor, OPC (P Cor.), OPC (P Cor.), Amb. Impactor, Amb. Impactor, Amb. Impactor, Amb. Impactor, Amb. Impactor, OPC acc., MCOPTICAL Part. C OPTICAL Part. C Volume Displace Data Analysis f OPC (P Cor.), I test lab: che Pulsed Flow Con Diffusion Batte Optical Part. C		Alternate Vender (AV), see Flow S.55-690			1.6
Amb. Low Fress Mass Train, for Mass Train, for Image Analysis Automated scree Lage Analysis SEM/EDS Interf.  Amb. Impactor, OPC (P Cor.),  Amb. Impactor, Amb. Impactor, OPC acc., MC OPTical Part. C OPTI	•	_	grams		-:
Mass Train, fo Mass Train, fo Image Analysis Automated scree Image Analysis SEM/EDS Interfi Amb. Impactor, OPC (P Cor.), Amb. Impactor, Amb.		35) 5 LP stages		AAA	5.3
Image Analysis Automated scree Image Analysis SEM/EDS Interfi Amb. Impactor, OPC (P Cor.), Amb. Impactor, Optical Part, C		5/17 Train, 3/4			7.1
Image Analysis Automated scree Image Analysis SEM/EDS Interfi Amb. Impactor, OPC (P Cor.), Amb. Impactor, Amb.		Std. Method 5/17 Train, 3/4 SCFM			7.7
Automated scree Image Analysis SEM/EDS Interfi Amb. Impactor, OPC (P Cor.), Amb. Impactor, Amb.		Image Analysis	ZZZ	222 10+h	TAN
Automated scree Image Analysis SEM/EDS Interfi Amb. Impactor, OPC (P Cor.), Amb. Impactor, Amb.			ZZZ	222	
Image Analysis SEM/EDS Interficable Dec (P Cor.), OPC (P Cor.), Amb. Impactor, Amb. Impactor, Amb. Impactor, Amb. Impactor, Amb. Impactor, OPC remote sens OPC acc., MC Optical Part. COPC (P Cor.), 1 test lab: che Pulsed Flow Condifiusion Batte Optical Part. COptical Part. COptical Part. COptical Part. COptical Part. COptical Part. COPTINE PLINTER PLOSER		5 Fr( 5 ->850), any mesh, dry	SIV	L:Oth	4.0
Amb. Impactor, OPC (P Cor.), Amb. Impactor, Optical Part. C	•		222	222	,
Amb. Impactor, OPC (P Cor.), Amb. Impactor, Amb. Impactor, Amb. Impactor, Amb. Impactor, OPC remote sens OPC acc., MC Optical Part. C Volume Displace Data Analysis f OPC (P Cor.), 1 test lab: che Pulsed Flow Con Diffusion Batte Optical Part. C	by size	Tmage Analysis	1	L:Oth	74.5
Amb. Impactor, OPC (P Cor.), Amb. Impactor, Amb. Impactor, Amb. Impactor, Amb. Impactor, OPC remote sens OPC acc., MCOptical Part. C Volume Displace Data Analysis f OPC (P Cor.), 1 test lab: che Pulsed Flow Con Diffusion Batte Optical Part. C	275	torphotogy crasses (etc. chem vs	s size) MA	MA 7.2.7.	72.0
		11 Fr( .05-> 35), QCM, P	AMBIENT I:CI		10.5
			222		
	E.	FitFr(.005->5)	0: PC	L:LS	22.5
			222	666	
	Microbal. 1	Fr( .05-> 25), QCM,	AMBIENT I:CI	AAA	15.0
	on SEM stud 3	Fr( .05-> .3), for SEM,			2
	t I C		222	222	
OPC remote sensor, Airborn, Req. OPC acc., MCA 24Ch, Data R. & Optical Part. Ct., Airborn, CleanRc Volume Displacement of Electrolyt Data Analysis for Ta/II L/3 Coul. OPC (P Cor.), liquidborn test lab: chem. by size & Morph Pulsed Flow Condensation Nuclei C Diffusion Battery, Tubular Optical Part. Ct., Airborn, CleanRo Printer ploter acc. for Faley O	& 3575	Full Spectrum MCA	PHA	MA	7.6
OPC acc., MCA 24ch. Data R. & Optical Part. Ct., Airborn, CleanRo Volume Displacement of Electrolyt Data Analysis for Ta/II L/3 Coul. OPC (P Cor.), liquidborn test lab: chem. by size & Morph Pulsed Flow Condensation Nuclei C Diffusion Battery, Tubular Optical Part. Ct., Airborn, CleanRo Printer ploter acc. for Faley O			222	222	
Optical Part. Ct., Airborn, CleanRo Volume Displacement of Electrolyt Data Analysis for TA/II L/3 Coul. OPC (P Cor.), liquidborn test lab: chem. by size & Morph Pulsed Flow Condensation Nuclei C Diffusion Battery, Tubular Optical Part. Ct., Airborn, CleanRo Printer ploter acc. for Faley O	& print	707 /-6- ) 11	0:A	AAA	4.9
Volume Displacement of Electrolyt Data Analysis for TA/II L/3 Coul. OPC (P Cor.), liquidborn test lab: chem. by size & Morph Pulsed Flow Condensation Nuclei C Diffusion Battery, Tubular Optical Part. Ct., Airborn, CleanRo Optical Part. Ct., Airborn, CleanRo Optical Part. Ct., Airborn, CReanRo Printer ploter acc. for Faley O Printer ploter acc. for Faley O		6 Fr( .3-> 10)	PHA O.b	MA	ر. و ، ر
			222	2.2.2	?
7		16 Fr(0.3->800), selectable	RP	57:1	28.1
	ctr.	Includes Apple comp. & DR software		MA	· }
	65	65 Fr(.003->3)	0: PC	L: LS	
			222	222	
	& Morph.; SEM M	Monolayer by dilute liquid suspe	suspension IAN	L:Oth	.250
		•		222	
l Part. l Part. l Part. r ploter		<pre>1 Fr(.002 -&gt; 1) Pulsed Flow, Conc. 1 Fr(.005 -&gt; .1) Threshold twne.</pre>	nc. only CNC	AAA	7.8
l Part. l Part. l Part. r ploter				2.2.2.	<b>7.</b> 2
ı Fart. 1 Part. r ploter	leanRoomMont 2	Fr( .5->	0:A	AAA	4.0
r ploter	1 ACFM	÷.	0:A	AAA	10.0
1000		^-?·		AAA	7.5
•		Frint & plot only, MCA in sensor pkg.	: pkg. MA	MA	7.5

		i	1	!	Inst.		v,
KEY					Type	Use	Quote
. No.	Vender/Model No.	Other Numbers:	DESCRIPTION/Comments	Key Parameters	Code	Code	x 1000
1550	KD-01 Diluter		10:1 Diluter for use with any OPC		MA	MA	8.
	* Fisher Foundry Inc.				222	ZZZ	
1610	* BAHCO Classifier	No. 6000	ASME PTC-28 procedure for Terminal Vel.	8 Fr(2,2' -> 54)	CET	L: AR	9.1
	4	11 11 11 11 11 11 11 11 11 11 11 11 11	•		777	777	,
1710		#55-500	Stk	9 Fr(F, .5 -> 10)	I:CI	FG: I	5,3
1720	Mark 4		Multi Jet Cascade Impactor, Iso. Stk Smp	$8 \text{ Fr}(F_{1,5} -> 7)$	I:CI	FG: I	5.8
1730	Right Angle Pre.Co		Right Angle Impactor Precollector	1 Fr( 11 at 0.5 SCFM), several grams	I:A	FG:I	1.6
1740		# 65-600	Cyclone Set w/ SoRI 1,2,3,4,5,F	Alternate Vender (AV), see Sierra 285-K	CXC	FG: I	7.6
1750	4-Stage Cyclone	#65-610	Cyclone Set w/ SoRI 1, 3, 5,F	Alternate Vender (AV), see Sierra 283-2K	CXC	FG: I	4.7
1760	3-Stage Cyclone	#65-620			CYC	FG: I	:
	* General Eletric Ord				ZZZ	ZZZ	
1810	CNC-2		Pulsed Flow Condensation Nuclei Counter	0 Fr(.001 -> .1) Pulsed Flow, Conc. only	CNC	AAA	10,3
	* Gilson:				ZZZ	ZZZ	
1910	Gilson Sieve Shakr	SS-8R	Priced w/Mesh 60,100,200,& 325 + SV8 P	Holds 8 sieves at a time	SIV	L:Oth	1.3
1920	Comp-sieve Anal.Sy	CP-2	n for Autom.	& print/plot	MA	MA	7.8
1930	ATM sonic Sifter	AT-3	(see ATM) alt. Vender	Alternate Vender (AV), see ATM	SIV	L:0th	4.0
1940	Laser Particle Cou	SA-1000	OPC (F Dif.), liquidborn	old Control	0:1	L:LS	10.2
1950	Particle Profile	SAA-3	Data analysis Acc. for SA-1000			MA	7.9
1960	Fritsch Pipette CF	SA-50	Manual Centrifugal Sedimentation Sizing	spen.	CSED	L:LS	7.0
1970	Cyclosizer Analyzr	SA-150	Liquid Suspension, Cyclone Set			L:LS	22.8
1975	Bahco Classifier	SA-160		(AV), see Fisher Found.	CET	AV	10.4
1980	Infrasizer, Gilson	SA-180		100 gm/hr rate	Misc	L: AR	6.4
1985	Photo Micron Sizer	#SA-2000S	Automated Spirometer, Centrifugal Sedim	many Fr(.01->500) Liquid Suspension	CSED	$\Gamma: \Gamma S$	20.9
		#SA-40	Glassware for Manual Sedimentation Ext.	Manual technique (1-> 100), Stokes Law	GSED	L:LS	
	* HIAC/Royco:				222	ZZZ	
2010		Main Frame		full data analysis, .3um->600um setable	PHA	MA	9 9
2020		w/sensor 1100	(scatter), airborn; CRM,	1100 Sensor, 6 Fr(.5->20) 1cfm	0:A	AAA	7.7
2030	4102	w/sensor 1200	(scatter), airborn; CRM,	1200 Sensor, 6 Fr(.5->20).1cfm or .01cfm	0:A	AAA	8.7
2040	Model 4130 System	w/sensor 1000A	OPC (scatter), airborn; CRM, 4100 w/sen.	cfm	0:A	AAA	14.0
2050	Model 5100	(stand alone)	Optical Part. Ct., Airborn, CRM stand al.	stand alone, 25-10um, 1cfm,	0:A	AAA	9.8
2051	(cont)	cont.		cont.	0:A	AAA	cont.
2060	4103			Sensor, GFr( 1->300), batch	0:1	r:rs	
2070	_	w/sensor 346	(scatter), liquidborn; 4100	346B Sensor, 6Fr(0.4->25), batch	0:1	$\Gamma: \Gamma S$	17.0
2080		ĕ		data analysis, 1-9000um setable	PHA	MA	ຜູ້
2080	HIAC 4313 System	W/sensor 346	(scatter),	4->25)		r:rs	22.9
			OPC (P Cor.), Liquidborn	64 Fr(.005->3), CRT	<i>7</i>	L: LS	27.9
	* Horlba:					222	
			Automated Spirometer, Centrifugal Sedim	many Fr(.02->100) Liquid Suspension	0	L:LS	22.0
	* In Tox:				222	ZZZ	
2210	5-Series Cyclone		Cyclone Set w/ SoRI 1,2,3,4,5,F	(AV), see Sierra 285-K	CXC	FG:I	4.8
			Screen Diffusion Battery	10 Fr(.003 -> .3)	DB	AAA	
	* Joyce/Loebl(England				222	222	
2310	Disk Centrifuge 4	#7AA5300		nsion	CSED	r:rs	32.4
2320	DCF Data An. Pkg.	F910001	Software & Interface Hardware for Apple	Disk Centrifuge	MA	æ :	4.0
2330	Apple lie comp.	F 003403	Computer, nardware only, W/ printer	Major Acc for Disk Centrifuge	W.	Æ	2.6

Table A-3: Manufacturer's Model Numbers

	\$ Quote x 1000	1 0	33.0	6.00	QUOTE	ł	57.0	c c	22.5	29.5	23	•	2.1	23.8	NAT	i	IAN	o u	6.0	6.3	1.7		IAN	20.4		46.0	13.5	15,3	3.0	o • 6	21.1	21.1	QUOTE	 	)		7.8
	Use Code	222	5.1.1 2.1.5	22.2	FG: I	222	L:Oth	222	Lils	L:LS	222	222	FG: I	ZZZ	222 L:0th	ZZZ	L: Oth	ZZZ MB	A	MA MA	MA	222	Lioth	ZZZ L:LS	222	FG: I	AAA	AAA	222 FG: I	FG: I	FG: I	FG:I	FG: I	FG: T	ZZZ	AAA	AZZ MA
	Inst. Type Code	ZZZ	0.50	222	O:FD	222	IAN	222	: : :		222	222	I:CI	ZZZ GSED	ZZZ	222	IAN	ZZZ DH3	41.7	MT17	MT17	222	IAN	222 RP	ZZZ	0:A	4 . 0 0	O:A	1:CI	I:CI			I:CI	T:A	222	0:A	424 MT17
PAGE: 3 of 4	Key Parameters	13 Ft (0 7-10g)	16 Fr(-12-> 42)		5 Fr(1.2-> 20), Outlets	,	ımage Analysıs / EDS	16 Fr(0,5->1800)		Cross Reference (CR) to 2600D for spec.	16 Fr(1,0->192)		$8 \text{ Fr}(F_{r, 5} -> 9)$	21 Fr( .1 ->100) Liquid Suspension	Image Analysis		Image Analysis	Full Spectrum MCA	4	Method 5/17 Train, 3/4	Mth. 6 Control Box, for Low Flow Imp.		ımage Analysıs	128Fr(0.3->1900)selectable			16 Pr(	-	8 Fr(F, 3 -> 10)	12 $Fr(F, 2 \rightarrow 20)$	stk sampler, 6 Low P	15 Fr(F,.05-> 20), stk sampler, 6 Low P S		t 0.5 AC	100 L	O* ET (O:01) ZO)	Std. Method 5/17 Train, 3/4 SCFM
	DESCRIPTION/Comments	OFC (F Dif.), liquidborn	OPC (F Dif. & side scattering), liquidb.		Optical Particle Counter, Airborn ,Stk.	Image Analterie		OPC (F Dif.), airborn w/acc. for liquid	(P Cor.), liquidborn	OPC (F Dif.), liquidborn	OPC (F Dif.), liquidborn		Multi Jet Cascade Impactor, Iso. Stk Smp	Automated Sedimentation Sizing, X-ray	Image Analysis		Image Analysis	MCA 4K channels, w/CMOS		Train, for running	Mass Irain, for running impactors, etc.	Image Apalvsis		Volume Displacement of Electrolyte		Optical Farticle Counter, Airborn ,Stk.			Jet Cascade Impactor, Iso. Stk		pressure & low press.	Js Wireyurar pressure & low press. Imp High Grain loading Imp. Inlats om/stag	Right Angle Impactor Precollector	Used as a Right Angle Impactor Precoll.	Optical Part, Ct. Birkorn recoved		Mass Train, for running Impactors, etc.
Manufacturer's Model Numbers	Other Numbers:												MRI Model 1502							000	7-077				100	001-0001											#201108
Table A-3: Manufe	Vender/Model No.	Leeds & Northrup: Microtrac 7995-10			Stack Part, Monit,	* Lemont: DA-10	Σ	2600D Spray D Any	Autosizer II	Marco Scientific.		ш	Migromeritics:	Sedigraph 5000ET	Image Any.	4	Magiscan 2 Nuclear Data Inc.	ND 62 MCA	Z	Nutech 2010		Image Any. System	Particle Data Inc.:	180LSD/ADC-80XY/KP	rarticle measuring	LPC-101	LAS-250X-CRT	Ħ		Mark 10	Mark 20B	MARK 8	Right Angle Pre.Co	BCURRA Cyc.	Follytec Optronics HN-15 Karlsruhe	Research Appliance	RAC Stacksamplr
	KEY No.	2400 <b>*</b> 2410		2500 *	2510	2610 *	2700 *	2710	2720	2800 *		* 5000 * 5000	3000 *	3010	4	ĸ	3300 *		*	3410	*		*	3610	•	3720		*	3810	3820	3840	3850	3860	3870	•	*	4010

		!	•	į	100		v
KEY						Use	Quote
No.	Vender/Model No.	Other Numbers:	DESCRIPTION/Comments	Key Parameters	1	Code x	x 1000
	* Sierra Inst. DAG			Z		222	
4110	Model 226		Multi Jet Cascade Impactor, Iso. Stk Smp	7 Fr(F, .9-> 14)	I:CI F	FG: I	5.9
4120	Model 228		Multi Jet Cascade Impactor, Iso. Stk Smp.	9 Fr(F, .3-> 18)	I:CI F	FG: I	3.8
4130	Model 2210		Sys w/regular pressure & low press. Imp	er, 2Low PS	I:CI F	FG: I	4.7
4140	Cyclade 285-K		Cyclone Set w/ SoRI 1,2,3,4,5,F	Fr(F, .3 -> 10), 10gm/stg. SoRI design	CYC FI	FG:I	7.1
4150	Cyclade 286-1K		Cyclone Set w/ SoRI 10, 1,2,3,4,5,F	Fr(F, .7 -> 15), 10gm/stg. SoRI design.	CYC F	FG: I	9.8
4160	Cyclade 286-2K		6	-> 15),10gm/stg. SoRI design		FG: I	8.8
4170	Cyclade 283-2K		Sori	design	CYC F	FG: I	4.7
4180	Model 220 CP		Cyclone design Impactor precollector	1 Fr( 9.2 at 0.25SCFM), several grams I	I:A F	FG: I	0.8
4200 *	* Southern Res. Inst.						
4210	SEDS	UFPS Diluter	Sample Extraction Dilution System	Stk Sampling, Amb 700F, 15:1-2000:1 D	DIL M	MA C	QUOTE
4250 +	* Spectrex:				Z ZZZ	222	
4260	ILI 1000	#6700000	OPC (F Dif.), liquidborn		_	L:LS	
4270	PPA-4	#6700810	PHA for ILI 1000 ,w/Apple Ile	ch MCA		МA	
4300	* Spectron Dev. Lab.:			2	Z ZZZ	222	
4310	Particle Sizing Interferometer	terferometer	OPC (Dual ), spray droplet type	DNA Fr(.5-> 25), cross stk.w/focused view O	O:FD F	FG: I	QUOTE
4400	* TSI:				Z ZZZ	222	
4405	EAA 3030	#3030	Elec. Aerosol Size Analy. w/o DR system	(Cross Ref.to EAA 3930 Sy for specs.)	EM A	AAA	20.8
4410	EAA 3930 SY	#3930	EAA 3030 w/ Apple soft. & computer			AAA	29.7
4420	DB/CNC 3931 Sy	#3931	DB, switching valves, & CNC w/o Apple	5 -> .2)		AAA	26.1
4430	DMPS/C 3932 Sy	#3932	EMC(Electro.MobilityClass), CNC, & Apple	->1.0)		AAA	42.0
4440	APS 33 SY	#3300I	Aerodynamic Particle Sizer w/o computer	48 Fr(.5 -> 15) A		AAA	29.5
4445	IBM-XT(DR for APS)	#3900XT	Data Reduction Hardware/Soft. for APS	computer & software	MA M	-	8.9
4450	CNC 3020	#3020	Continuous Flow Conden. Nuclei Counter	Flow, Conc. only	CNC AZ	AAA	17.0
4460	DB 3040	#3040	Screen Diffusion Battery, opt. Switch V			AAA	4.9
			Lab Diluter, accesory to the APS 33	cal output			3,7
4500 *	⊃				222 22	ZZZ	
			Image Analysis	Image Analysis I.		L: Oth	IAN
<b>4</b> 600 <b>*</b>	>			Z		222	
			Image Analysis	Image Analysis I.		L:Oth	IAN
4700 *	3			ž		ZZZ	
4710	Dawn Model B	:	OPC (F Dif.), liquidborn	16 Fr(0.6-> 50) 0	^	L: LS	17.0
		#1600-IV	Data Analysis, etc for DAWN	computer & software	PHA MA	_	2.5
<b>4</b> 800 *	N			72	222 222	Z	
	IBAS		Image Analysis	Image Analysis		L:Oth	IAN
	* Zoltec:					222	
4910	Brink Model C		Impactor, Low Flow (Inlet, High Loading)	8 Fr(F,.5 -> 9 )	I;CI FG	FG: I	2.9

Table A-4: Instrument Type Sorted: Description

Key Parameters	Alternate Vender (AV), see Fisher Found.  Alternate Vender (AV), see Fisher Found.  B Fr(.5> +5)  O Fr(.001-> -1) Pulsed Flow, Conc. only  O Fr(.001-> -1) Pulsed Flow, Conc. only  O Fr(.001-> -1) Pulsed Flow, Conc. only  O Fr(.01-> 5) Manual, Liquid suspension  many Fr(.01-> 60) Liquid Suspension  many Fr(.01-> 60) Liquid Suspension  Alternate Vender (AV), see Sierra 285-K  Fr(F., 3 -> 10), 10gm/stg. SoRI design  Fr(F., 3 -> 10), 10gm/stg. SoRI design  Fr(F., 3 -> 15), 10gm/stg. SoRI design  Fr(F., 3 -> 15), 10gm/stg. SoRI design  Fr(F., 3 -> 15), 10gm/stg. SoRI design  Fr(F., 005 -> .2)  10 Fr(.005 -> .2)  10 Fr(.005 -> .2)  10 Fr(.005 -> .2)  11 Fr(.005 -> .2)  12 Fr(.1 -> 100), 11quid Suspension  Alternate Vender (AV), see Flow 5.55-690  Fr(.003 -> 10)  1 Fr(.005 -> 2)  1 Fr(.1 -> 100), stokes Law  Alternate Vender (AV), see Flow 5.55-690  Fr(.1 -> 100) Liquid Suspension  Alternate Vender (AV), see Flow 5.55-690  Fr(.1 -> 100) Liquid Suspension  Alternate Vender (AV), see Flow 5.55-690  Fr(.1 -> 100) Liquid Suspension  Alternate Vender (AV), see Flow 5.55-690  Fr(.1 -> 100) Liquid Suspension  Alternate Vender (AV), see Flow 5.55-690  Fr(.1 -> 100) Liquid Suspension  Alternate Vender (AV), see Flow 5.55-690  Fr(.1 -> 100) Liquid Suspension  Alternate Vender (AV), see Flow 5.55-690  Fr(.1 -> 100) Liquid Suspension  Alternate Vender (AV), see Flow 5.55-690  Fr(.1 -> 100) Liquid Suspension  Alternate Vender (AV), see Flow 5.55-690	Fr(F,.5 -> 7)
\$ Quote x 1000 DESCRIPTION/Comments	Aerodynamic Particle Sizer w/o computer (See Fisher Foundery, Bahco) alt. Vendr ASME PTC-28 procedure for Terminal Vel. Pulsed Flow Condensation Nuclei Counter Manual Centrifugal Sedim Continuous Flow Conden. Nuclei Counter Manual Centrifugal Sedim Automated Spirometer, Centrufugal Sedim Automated Spirometer, Centrufugal Sedim Automated Spirometer, Centrufugal Sedim Cyclone Set w/ SoRI 1,2,3,4,5 Cyclone Set w/ SoRI 1,2,2,3,4,5 Cyclone Set w/ SoRI 1,2,2,3,4,5 Cyclone Set w/ SoRI 1,2,2,3,4,5 Cyclone Set	5.8 Multi Jet Cascade Impactor, Iso. Stk Smp 8
\$ Quote Other Numbers: x 1000	#3020 8A-160 No.6000 #3020 8A-50 #SA-2000S #7AA5300 #5A-2000S #7AA5300 #65-600 #65-610 #65-620 #65-620 #55-620 #55-690 #50-900 #55-690 #50-900 #55-690	200
Vender/Model No.	APS33 Bahco Classifier BAHCO Classifier Rich 200 CNC CNC-2 CNC CNC-2 CNC CNC-2 CNC CAPA-500 Spirom, Disk Centrifuge 4 SASS G-Stage Cyclone 3-Stage Cyclone 3-Stage Cyclone 5-Series Cyclone Cyclade 286-3K Cyclade 286-3	•
Manufacturer	TSI:  Gilson Fisher Foundry Inc. Brvironment One: General Electric Ord TSI: Gilson Gilson Gilson Gilson Gilson Gilson Flow Sensor Div. In Tox: Sierra Inst. DAG Gilson Environment One: TSI: TSI: TSI: TSI: TSI: TSI: TSI: TSI	
t. B Use Code	AAA AAA AAA AAA AAA AAA AAA AAA AAA AA	
Inst. KEY TYPE No. Code	1440 AT 1975 CET 1410 CNC 1410 CNC 14810 CNC 1985 CSED 2310 CSED 2310 CSED 0110 CYC 1750 CYC 1760 CYC 1770 CYC 1770 CYC 14140 CYC 14140 CYC 14140 CYC 1420 DB 1420 DB 1420 DB 1420 DB 14410 EM 16210 EM 16210 EM 16210 EM 16210 EM 16210 EM 16210 EM 1720	

!		ρ,	S D4			S				E C							e)		÷		lot Lot						•								:fm			cont.		
Key Parameters	8 Fr(F,.5 -> 9) 8 Fr(F,.3 -> 10)	12 Fr(F,.2 -> 20) 28 Fr(F,.05-> 20), stk sampler,6 Low	, stk	DNA Fr(F,1 -> 10)	7 Fr(F, .9-> 14)	9 Fr(F, .3=> 18) 11 Fr(F,.09=> 28), stk sampler,2 Low P	8 Fr(F, 5 -> 9 )	Image Analysis	Image Analysis	Monolayer by dilute liquid suspension	Image Analysis / EDS	Image Analysis	Image Analysis	Image Analysis	Image Analysis	Image Analysis	Morphology Classes (el. chem vs size)	Includes Apple comp. & DR software	Print & plot only, MCA in sensor pkg.		Inc. Computer, DR software, & print/plot	Major Acc for Disk Centrifuge	Major Acc for Disk Centrifuge	Std. Method 5/17 Train, 3/4 SCFM		Std. Method 5/17 Train, 3/4 SCFM	Mth. 6 Control Box, for Low Flow Imp.	std. Method 5/17 Train, 3/4 SCFM	Ŀ	16 Fr( .3-> 20) 6 Fr( .3-> 10)		÷.	.3-	1100 Sensor,6 Fr(.5->20) 1cfm	1200 Sensor, 6 Fr(.5->20).1cfm or .01cfm	1000 Sensor,6 Fr(.3->15) 1cfm	stand alone, .25-10um, 1cfm,		4 FI ( .1-710 ) 16 Fr ( .2->12 )	
\$ Quote x 1000 DESCRIPTION/Comments	Multi Jet Cascade Impactor, Iso. Stk Multi Jet Cascade Impactor, Iso. Stk	3.9 Multi Jet Cascade Impactor, 180. 5tk 5mp 21.1 Sys w/reqular pressure & low press. Imp	Sys w/regular pressure & low press.		Multi Jet Cascade Impactor, Iso. Stk	3.8 Multi Jet cascade impactor, 180. Stk Smp 4.7 Svs w/reqular pressure & low press. Imp		IAN Image Analysis	Ħ	.250 test lab: chem, by size & Morph.; SEM	5/.0 Image Analysis	IAN IMAGE ANALYSIS TAN Tmace Analysis			IAN Image Analysis			DNA Data Analysis for TA/II L/3 Coul. ctr.		.8 10:1 Diluter for use with any OPC	7.8 Electronic Bal. System for Autom. Sieve	4.0 Software & Interface Hardware for Apple	2.6 Computer, hardware only, w/ printer 8 0 hata beduction hardware/coft for hos	-	7.7 Mass Train, for running Impactors, etc.		Mass			4.9 OPC remote sensor, Airborn, Req. 8040 7.5 Optical Part, Ct. Birborn CleanRoomMont		Optical Part.	Optical Part.		8.7 OPC (scatter), airborn; CRM, 4100 w/sen.	14.0 OPC (scatter), airborn; CRM, 4100 w/sen.	Optical Part. Ct., Airborn, CRM stan	cont.	13.3 Optical Fart. Ct., Alrocin, CRM 15.3 Optical Part. Ct., Airborn, CRM	
Other Numbers: x	MRI Model 1502																					F910001	#3900 vm				220-2	#201108	SA-180					w/sensor 1100	w/sensor 1200	W/sensor 1000A		cont.		
Vender/Model No.	. 7	Mark 5 Mark 10	Mark 20B	w		Model 228 Model 2210		Image Analysis	Omnicon 3500	CCSEM (Test Lab)		Image Any. System Magican 2	Image Anv. System	0	Image Any, System	IBAS	EM-2	Coulter Accucomp	FP-303 Opt.		Comp-sieve Anal.Sy	DCF Data An. Pkg.	Apple IIe Comp.	Emission Param, An	Universal Stack Sp	Nutech 2010	Nutech 220-2	RAC Stacksamplr	Intrasizer, Gilson	Model 226 Model 8060	Status 2100	Status 4000	Status 5000	Model 4101 System		Model 4130 System	Model 5100	(cont)	LAS-250X-CRT	
Manufacturer	Belfort Pollution Control	Pollution Control	Pollution Control	Pollution Control	Sierra Inst. DAG	Sierra Inst. DAG	Zoltec:	Artek Systems Corp	Bausch & Lomb:	Energy Technology		Munnall CO. The:	Optomax:	Unitron	Varian:	Zeiss:	Bausch & Lomb:	Coulter:	Faley Internat.:	Faley Internat.:	Gilson	Joyce/Loebl(England	Joyce/Loebl(England	Andersen Samplers	Andersen Samplers	Nutech Corp.	Nutech Corp.	Research Appliance	Gilson	Climent:	Faley Internat.:	Faley Internat.:	Faley Internat.:	HIAC/Royco:	HIAC/Royco:	HIAC/Royco:	HIAC/Royco:	HIAC/Royco:	Particle Measuring Particle Measuring	ı
Use Code	FG: I	FG: I	FG: I	FG: I	FG: I	FG: I	FG:I	L:Oth	L:Oth	Lioth	L:Oth	1.051	L.oth	L:Oth	L:Oth	L:Oth	ΑA	MA	ΜA	MA	MA	Æ	AN AN	E W	Æ	MA	ΜĀ	MA	L: AR	AAA	AAA	AAA	AAA	AAA	AAA	AAA	AAA	AAA	AAA	
Inst. Type Code		ici				I:CI		IAN	IAN			TAN			IAN	IAN	ΑA		W.	MA			¥ £			MT17	MT17			4 . 0 0			0: <b>A</b>	0:A	0:A	0:A	0:A	0: <b>A</b>	<b>e e</b> :0	
KEY No.	2910	3830	3840	3850	4110	4130	4910	0410	0610	1310	2610	3310	3510	4510	4610	4810	0620	1220	1540					0360	0370	3410	3420			1110									3730	

Table A-4: Instrument Type Sorted: Description

Key Parameters	46 Fr(0.5-> 20) 60 Fr (4->11) 16 Fr(0.5-> 1800) 5 Fr(1.2-> 20), Outlets DNA Fr(2.5-> 25), cross stk.w/focused view 13 Fr(0.7->125) Cross Reference (CR) to 2600D for spec. 16 Fr(0.5->100) 16 Fr(0.6-> 50) 17 Fr (1.0->192) 18 Fr(0.6-> 50) 19 Fr (0.5->100) 19 Fr (0.5->100) 19 Fr (0.5->100) 10 Fr (0.5->100) 11 Fr (1->100), Threshold Control 1000 Sensor, 6Fr (1->100), batch 1000 Sensor, 6Fr (1->25), batch 1000 Sensor, 6Fr (1->25) 1000 Sensor, 6Fr (1->25) 11 Fr (1->100) 12 Fr (0.05->5) 15 Fr (0.05->5) 16 Fr (0.05->5) 17 Fr (1->->->->->
\$ Quote x 1000 DESCRIPTION/Comments	DNA Optical Part. Ct., Airborn, research 46.0 Optical Particle Counter, Airborn, 5tk. 28.0 OPC (F Dif.), airborn w/acc. for liquid 20.0TE Optical Particle Counter, Airborn ,Stk. 28.0 OPC (F Dif.), liquidborn 33.0 OPC (F Dif.), liquidborn 3 OPC (F Dif.), liquidborn 3 OPC (F Dif.), liquidborn 3 OPC (F Dif.), liquidborn 17.0 OPC (F Dif.), liquidborn 17.0 OPC (Scatter), liquidborn 22.5 OPC (P Cor.), liquidborn 3.9
\$ Quote Other Numbers: x 1000	#6700000  #6700000  SA-1000  W/sensor 346  W/sensor 346  W/sensor 346  #/sensor 346  #/sensor 346  #/sensor 146  #
Vender/Model No.	PPSSS 2600D Spray D Any Stack Part, Monit. Particle Sizing Interferometer Microtrac 7995-10 7995-30Small Part. Model 3600E Granulometer ILI 1000 Dawn Model B Laser Particle Cou SA-1000 Model 4103 System w/sensor 30 Model 4113 System w/sensor 3 HIAC 4313 System w/sensor 3 HIAC 4313 System w/sensor 3 HIAC 4313 System w/sensor 3 HIAC 4310 System w/sensor 3 HIAC 4310 MAD Series 35+ Model 4100 Mutcobp Model 270 Mutcosizer II MAC Series 35+ Model 8040 Main Frame HIAC 4300 Main Frame MO 62 MCA Particle Profile Main Frame HIAC 4300 Main Frame
Manufacturer	Polytec Optronics Particle Measuring Malvern: Leeds & North. Res Spectron Dev. Lab.: Leeds & Northrup: Malvern: Malvern: Wyatt Technology Gilson HIAC/Royco: HIAC/Royco: HIAC/Royco: Malvern: Coulter: Coulter: HIAC/Royco: Malvern: Coulter: Gilson HIAC/Royco: Malvern: Coulter: Gilson HIAC/Royco: Malvern: Coulter: Gilson HIAC/Royco: Malvern: Goulter: Gilson HIAC/Royco: Walvern: Gilson HIAC/Royco: Walvern: Gilson HIAC/Royco: Wolear Data Inc. Spectrex: Wyatt Technology Coulter: Faring
Use	AAA  AAA  AAA  FG:I  FG:I  L:IS  RAA  MA  MA  MA  MA  MA  MA  MA  MA  M
Inst.	0 0:A 0 0:B 0 0:E
KEY No.	3910 2510 4310 2430 2430 2420 2730 2730 4700 1920 2000 2000 2000 1920 1950 1950 1950 1950 1950 1950 1950 195

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Comments continued (3 of 3)				en Pipet method into submicron range.		Size is operator selectable.													sample for amb.inst. (.01-1.5 micron)	Aerosols. Capilary diluter, fixed, 20,100.	CR	F 0000 mile a familiar at 25, and 25,	outer hardware/data analysis pkg 3900-/1 Oty of extract. sets qty of size cuts.	by X-ray attinuation							Crystal Microbalance	Crystal Microbalance			(**** 6 04)		Metrology Res. Inc. was bought by Belfort	Univ. of Washington design
Comments continued (2 of 3)	AV	1.0 gm/cc. Terminal Settling Velocity instrument (DB,EM,etc.).	instrument (DB, EM, etc.).	Sizing must be performed by a separate — instrument (DB,EM,etc.). Conc. by dry weight, size by run time and radius at Pipette point. Extends Andreasen Pipet method into submicron	ifuge. Concentration by photo-extention.	Computer controled centrifuge. Concentration by photo-extention.	inge: Concentration by photo-textention: cordanics module (\$ +8.3K) accessory				7.5)	8.5, 15); 15um IP	11 , 15); 15um IP				COOL CIME LINE	and CNC 3020	ng use. Extracts, dilutes and conditions	Lab diluter (Amb.) intended as an accessory for the APS 33 for high concentration	CR		d comp	cond			Angle, SORI/EPA design.	***************************************	Angle, SORI/EPA design.	2.0, 3.3, 6.6, 10.5, 15.7, 21	2.1, 4.3, 8.8, 18, 35) Mfg	2, 6.4, 12.5, 25) Mfg Quartz	1.2,	5,9		3, 6.8, 10.2, ker 18, built in Freseperator 3. 6.8) Ref 18, same as Mark 3 except uses	9.0) Ref 18, stage 1 & 2 cut at 9.0	10.1) Ref 18, stage 1 & 2 cut at 10.1
Comments (1 of 3)	(.5, .54, .58, -> 15 by 1.075 ratio ) AV	(2.2, 3.5, 7, 13, 21, 36, 48, 54) for Sizing must be performed by a separate				Import, Japan. Computer controled centrifuge. Concentration by photo-extention.	<pre>Import, England. Computer controled central 3 cyc set + F, 4 SCFM (10,3,1,F) with an</pre>	AV	AV	1.0 ACFM, 300F (F, .57, 7.5)	1.0 ACFM.300F (F57, 1.1.:2.7, 3.5.				O.			Includes DB 3040, Switching Valve 3042, Used with DB/CNC System 3931, screen DB's	Prototype system designed for stk. sampl	Lab diluter (Amb.) intended as an access	Cross Reference (CR)	0.14 SCFM(.0042, .0075, .0133, .024,.042	Includes Electrostatic Classifer 3071, CNC 3020 for low concentrations an Extract dilute liquid suspension at different time intervals, dry and weigh.		AV	for Loadings > 1	Designed for Loadings > 1 gr/SCF, Right		Designed for Loadings > 1 gr/SCF, Right	0.1 SCFM (F,.08, .11, .23, .52, .9, 1.4,		0.01SCFM (F,.05, .1, .2, .4, .8, 1.6,3.2,	0.0/SCFM (F., US, 3, 2) ML9 0.5 ACFM.1200F(F18284361, .92,	0.5 SCFM (F, .42, .78, 1.2, 2.2, 4.3,	SCFM (F, 1.5, 5.8, 11) SORI	0.5 SCPM (F.,52, .90, 1.3, 2.2, 3.0, 4.5, 0.5 SCPM (F.,52, .90, 1.3, 2.2, 3.0, 4.3,	SCFM (F, .52, .69, 1.1, 2.2,	SCFM (
Vender/Model No.	APS 33 Sy BAHCO Classifier	BAHCO Classifier Rich 200 CNC		CNC 3020 Fritsch Pinette CF	Photo Micron Sizer	CAPA-500 Spirom.	SASS	6-Stage Cyclone	4-Stage Cyclone	3-Stage Cyclone	Cyclede 285-K	Cyclade 286-1K	Cyclade 286-2K	Cyclade 283-2K	Cyclosizer Analyzr	Diffusion Denuder	9061	DB/CNC 3931 SY	ŭ	Diluter 3302	EAA 3030		DMPS/C 3932 Sy	Sedigraph 5000ET	Right Angle Pre.Co	Preseparater, St.	Right Angle Pre.Co	RIGHT ANGLE FRESCO	Model 220 CP	Low Pressure Imp	C-2000 QCM Cascade	PC-202 QCM	MPS-3 APT HTP Impactor	Mark III Impactor	HCSS Impactor	Mark 3	Belfort 1502	Mark 3
Use Code	AAA	L: AR AAA	AAA	AAA 1.:TS	L:LS	L:LS	L:LS FG:E	FG:I	FG: I	FG:I	1.04	FG:I	FG: I	FG: I	r:rs	AAA	A P	AAA		£ £	AAA	AAA	AAA	Lits	AV	FG: I	FG:I	FG:1	FG:I	AAA	AAA	AAA	AAA FG.T	FG:1	FG:I	FG:I	FG: I	FG: I
Inst. Type Code	4440 AT 1975 CET	1610 CET		4450 CNC 1960 CSED			2310 CSED 0110 CYC			1760 CYC								4420 DB	4240 DIT			4410 EM	4430 EM					3850 I:A			0710 I:CI		0920 I:CI				2910 I:CI	

Comments continued (3 of 3)	Stages interchangable with Mark 3  Loading collection stages available.	class and analy., redefine and reanaly.	class and analy., redefine and reanaly.	cuts (x .707), Stokes Law	5mw HeNe laser angle, HeNe open cavity laser cont.  Laser Particle Counter  Laser Aerosol Spectrometer  MCA, liquidborn opt., no pump-passive flow (2->11 by .6), open sensor section.  feed, mirco. control, no pump-passive flow
Com		class	class	cuts (	
Comments continued (2 of 3)	High Loadings, custom order.  Low Loadings, custom order.  High Capacity Stack Sampler  Ref. 18  18 ) Mfg. Data  4.2, 6.9, 17, 28 ) Mfg Data  , 9.2 ) Ref. 18, Low Flow, Inlets, High	each particle is stored on disk. Define	each particle is stored on disk. Define (PCA II), 100 ch , selectable with comparable flow rate	sampling train (Flow control, trav. etc.) of redispersed powder, (50-)100 gm),F+ 6 .8, 1, 1.5, 2, 3, 4, 5, 6, 7, 8, 9, 10) 1, 5, 10), RS 232C, alarms, temp., w/o printer	Near forward scattering Near forward scattering Filipsoidal Mirror 30->170 deg. Elipsoidal Mirror 60->120 deg., right Facility Monitoring System 7, 5, 6, 8, 10, 12), printer, RS232C, MCA option, basic unit for interface to by .05),(1,15->5,65 by .3), (.5->2 by.1) Analyser, Acc. for liquidborn & dry power dual optics system, PROFOTYPE ONLY
Comments (1 of 3)	0.5 SCFM (F.21, .28, .36, .46, .62, .80 0.2 SCFM (F. DNA ) Inlets, Low Flow, 2.0 SCFW (F. DNA ) outlets, high Flow, DNA SCFM (F. DNA ) Inlets, High Flow, 0.25SCFM (F9, 1.7, 2.5, 4.1, 11, 14) 0.25SCFM (F3, .5, .9, 1.7, 2.7, 4.4,11 0.1 SCFM (F9, .35, .57, .86, 1.5, 2.7 0.3 SCFM (F47, .78, 1.1, 2.3, 3.7, 5.4	Morphology, size, & elemental chem. of	Morphology, size, & elemental chem. of Note: MCA acc. :Population Accessory II Also includes clock and RS 232 C May be used with any aerosol instrument	Mount Imp. or Cyc. to probe to complete Bulk powder seperation by Air Blutriation Remot, w/ 8040 Main Frame: (.3, .4, .6, Stand alone, replaces 208C,(.3, .5, .7, .7, .5, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .5, .1, .2, .5), 70 deg. side scatter (.3, .2, .2, .2, .2, .2, .2, .2, .2, .2, .2	Model number is a Pkg, 4100 + sensor Model number is a Pkg, 4100 + sensor Model number is a Pkg, 4100 + sensor (.25, .3, .5, 1, 5, 10) stand alone Aharm, opt. Printer and transducer, (.1, .3, .5, .1)  (.2, .3, .4, .5, .6, .8, 1, 1.2, 1.5, 2, .90 deg scattering, Halogen lamp, 64 ch A Ranges, 15 steps per range: (.4->1.15)  (3 ranges, 16ch/range), Spray broplet (.3, 1, 3.5, 7.5, 15), Fiber optics, co.
Vender/Model No.	Mark 5 Mark 10 Mark 10 Mark 208 Model 226 Model 228 Model 2210 Brink Model C Image Analysis	Omnicon 3500 CCSEM (Test Lab) DA-10 Image Any. System Magiscan 2 Image Any. System Model 1A1000 Image Any. System	EM-2 Coulter Accucomp FP-303 Opt. KD-01 Diluter Comp-sieve Anal.Sy DCF Data An. Pkq. Apple IIE Computer TRM-writto for Anal	Emission Param. No. N. V.	
_	FG:I FG:I FG:I FG:I FG:I FG:I	r.oth r.oth r.oth r.oth r.oth r.oth	MA MA MA MA MA	MA MA MA MA MA MA AAA AAA AAA	
	3820 I:CI 3830 I:CI 3840 I:CI 3850 I:CI 4110 I:CI 4130 I:CI 4910 I:CI 9910 I:CI	IAN IAN IAN IAN IAN IAN IAN IAN	0620 MA 1220 MA 1540 MA 1550 MA 1920 MA 2330 MA 4445 MA	MT17 MT17 MT17 MT17 MT17 M15C O:A O:A O:A	2030 0:A A 2040 0:A A 2050 0:A A 2051 0:A A 3720 0:A A 3730 0:A A 3710 0:A A 2710 0:P B 2510 0:P FC

ents continued (3 of 3)	conf. Transfer and Utilization of	CR hardware, plotter etc.)			ch MCA, printer/plotter, DR, RS232C,etc.	ch MCA, printer/plotter, DR, RS232C,etc. ch MCA, printer/plotter, DR, RS232C,etc.	Apple w/ printer, software, etc. computer/printer for data storage & anal	AV
Comments continued (2 of 3)		CR Computer opt, available (software, scattering, bottled samples Columbia MPC (PHA & DR)	Light obscuration sensor	.10->.30, .20->.60, .40->1.2, .80->3.0 DR computer/printer		temp, humidity), Main Frame includes 6 temp, humidity), Main Frame includes 32	or (13-> 100 in 5 um steps), includes (2% to 50% of orifice diameter),includes (2% to 50% of orifice diameter),includes	AV
Comments (1 of 3)	Argone Lab., Dual Optics (ratio & Interferometry), PROTOTYPE, 1978 Denver EPA (.7->125 by x1.414 steps) (.12, .17, .24, .34 by 2nd optics sys., F Diff.; .43->42.2 by x1.414 steps)	Same as 2000 Dat dailying 10, 11910 (1, 1.5, 2, 3, 4, 6, 8, 12, 16, 24), 15 ch McA by Acc. PPA-4, multiangle Laser, multi angle scattering, Acc.: See Maior Acc.: SAA-3 for 16 ch McA)	Model number is a Pkg, 4100 + sensor Model number is a Pkg, 4100 + sensor Model number is a Pkg, 4300 + sensor fitted curves, unimodal	<pre>5 ranges (13 div/range) .04-&gt;.15, (Fitted curves , multimodal, includes 32 pt fitted curve</pre>		ext. sensors (particles, ext. sensors (particles,	W/LLL 1000: (1-7 ) / In 1 um Steps) Select orifice, 16 ch for this orifice Select orifice, 124 ch for this orifice	AV
Vender/Model No.	Particle Sizing In Microtrac 7995-10 7995-30Small Part.	model 5000 Granulometer ILI 1000 Dawn Model B Laser Particle Cou	Model 4103 System Model 4113 System HIAC 4313 System BI-90	N4-128/MD NICOMP Model 270 Autosizer II MCA Series 35+	Model 8040 Particle Profile	HIAC 4300 ND 62 MCA	Columbia MPC TA II L/3 Plus 180LSD/ADC-80XY/KP L3P Sonic Sifter	Gilson Sieve Shaker ATM sonic Sifter
. Use Code	FG:I L:LS L:LS	1:12 1:13 1:13 1:13	L:LS L:LS L:LS L:LS	L:LS L:LS L:LS MA	MA AM	MA MA	MA L:LS L:Oth	r:oth
Inst. KEY Type No. Code	4310 O:FD 2410 O:FD 2420 O:FD 2730 O:FD		2060 O:L 2070 O:L 2085 O:LB 0810 O:PC	1230 0:PC 2090 0:PC 2720 0:PC 1010 PHA	1120 PHA 1950 PHA 2010 PHA	2080 PHA 3310 PHA 4270 PHA	4720 PHA 1210 RP 3610 RP 0510 SIV	1910 SIV 1930 SIV

Table A-6: Instrument Type Sorted: Specifications

1 of 3

PAGE:

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N/A CR N/A	N/N N/N VA / 1/2 2/1/2	N/N N/2 1/2 1/2 1/2 2/2 2/2 2/2 2/2 2/2 2/2 2
N/A N/A N/A	N/A N/A AV 1/8 3/16	3/32 N/A N/A N/A 1/8
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CR 21.8	N/A N/A A/A 75 .45	35 10 10 70 75 75
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930 Sy 1932 Sy 19 Pipe	Pre.C r,St. Pre.C	Model 220 CP Low Pressure Imp C2000 QCM Cascade PC202 QCM MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3 MPS-3
er 330 030 3 c 3 asen 8	raph 5 Angle parate Angle Angle Angle	Model 220 CP Low Pressure Imp C-2000 QCM Casca PC-202 QCM APF ITP Impactor MARK III Impactor HCSS Impactor
Dilut EAA 3 EAA DMPS/0	Sedig Right Prese Right Right BCURR	Model Low Pr C-2000 PC-202 MPS-3 APT HT Mark I
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AAA AAA S.LS	7.1.58 7.1.58 7.1.66 7.1.66 7.1.66	5 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
DIL MA EM AAA EM AAA EM AAA EM AAA GSED L:LS		
00/ 7 W/N W/N C. C. W/N	N/A	N/A

A-17

Table A-6: Instrument Type Sorted: Specifications

3 of 3

PAGE:

Power (amp)	cont.	\$	<b>\$</b>	<b>&lt;</b> 2	10	\$	20	<5	'n	2	<u>გ</u>	\$	ŝ	\$	\$	<b>\$</b>	\$	\$	\$	<b>\$</b>	<b>&lt;</b> 5	<b>&lt;</b> 2	\$	<b>&lt;</b> 5	<b>\$</b>	\$	<b>&lt;</b> 2	<b>\$</b>	<20	\$ 5	\$	\$	\$	<b>\$</b>	ΑV
Weight (1b)	cont.	45	9	09	150(3)	70	154(3)		103(3)	103(3)	S,	127	31	45	20	<70	<70		75	70	165	70		40	35	26	73		40	40	100	100	09	100	AV
Max- Oper. Temp. Deg F	cont.	Amb	Amb	Amb	480	Amb	200	Amb	Amb	Amb	ಜ	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	Amb	AV
-min   Port Req.	cont.	N/A	N/A	N/A	4	N/A	4	N/A	N/A	N/A	S.	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	ΑV
(in.) able	cont.	N/A	A/N	N/A	N/A	N/A	A/N	N/A	N/A	N/A	S	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	ΑV
-Nozzle Sizes(in. Available min Max	cont.	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	S	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	AV
Nominal Flow Rate (SCFM)	cont.	٠.	٠.		N/A	N/A	N/A	N/A	N/A	N/A	CR	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	ΑV
ing-  e ) Max.	cont.	-	-	N/A	N/A	N/A	N/A	N/A	N/A	N/A	క్ర	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	ΑV
-Sampling- Rate (SCFM) min. Max.	cont.	-	-	N/A	N/A	N/A	N/A	N/A	N/A	N/A	CR	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	AV
ion -   wasis-   ) MAX.	cont.	1.4E7	1.4E7	1.55	5E4	DNA		1.0E7	N/A	N/A	೪	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	ΑV
Information -Number Basi (#/cm3) min. MAX	cont.	10	100	DNA	DNA	DNA	N/A	DNA	N/A	N/A	క్ర	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	AV
ration sis-  -	cont.	N/A	N/A	N/A	N/A	N/A	1000	N/A	N/A	N/A	క	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	AV
Concent: Mass Bas , (mg/M3 min, M	cont.	N/A	N/A	N/A	4-	N/A	10	N/A	N/A	N/A	CR	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	AV
Dia. Basis A,P,O	cont.	0	0	0	0	0	0	0	0	0	S	0	0	0	0	0	0	0	0	0	0	0	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	Other	Other	Other	Other	ΑV
COARSE >10	cont.	0	7		7		-		œ	S	S	6	7						0		0	0			13						J	J	S.		ΑV
on MED C 3->10	cont.	-	Ŋ	ple	15+14	ble	7		٣	m,	CR	e	7	ole	ole	ole	ole	o]e	0	ole	0	0	ole	ole	7	ole	ole	ole			ole	ole	0	0	ΑV
soluti FINE .3->3	cont.	7	œ	electable	15+15 15	electabl	-		ιΩ	9	CR	4	ო	electab]	electable	electabl	electabl	selectabl		electabl	many	many	electable	electabl	-	selectabl	selectabl	electabl			electabl	Jec	0	0	ΑV
#of ize UF uts 0->.3	cont.	-	7	Se	0	se	-		0	3	C,	0	0	se	se	se	Se	ΣÔ	ים	se	many	many	Se	Ø	0	Ø	Ω	se			se	S	0 (	0	ΑV
hof #of Size Cuts	cont. cont.	4	16	64	4 X1 5	16	ιΩ	DNA	13	16	చ	16	16	16	-	9	9	32	Fitted	65	64	32	4096	24	16	و	32	4096	DNA	DNA	16	124	.n.	ω ;	ΑV
Vender/Model No.	(cont)	LPC-101	LAS-250X-CRT	HN-15 Karlsruhe	FPSSS	2600D Spray D Any	Stack Part. Monit.	Particle Sizing In	Microtrac 7995-10	7995-30Small Part.	Model 3600E	Granulometer	ILI 1000	Dawn Model B	Laser Particle Cou	Model 4103 System	Model 4113 System	HIAC 4313 System	BI-90	N4-128/MD	NICOMP Model 270	Autosizer II	MCA Series 35+	Model 8040	Particle Profile	Model 4100	HIAC 4300	ND 62 MCA	PPA-4	Columbia MPC	TA II L/3 Plus	180LSD/ADC-80 XY/KP	L3P Sonic Sifter	Gilson Sieve Shakr	ATM Sonic Sifter
Use	AAA	AAA	AAA	AAA	FG: I	AAA	FG:I	FG: I	L:LS	L:LS	L:LS	Ľ:ĽS	L:LS	L:LS	$\Gamma:\Gamma$ S	L:LS	L:LS	L:LS	r:rs	L:LS	L:LS	r:rs	Ψ¥	Æ	W.	¥.	¥:	MA	W.	¥.	7:12 1:13	L:1.5	Lioth	Lioth	L:Oth
Inst. Type Code	0: A	0: <b>A</b>	0:A	0: <b>A</b>	0:A	O:FD	0:FD	0:FD	0:FD	0:10	0:FJ	0:10	0: FD	o: F	O:L	0:I	0:1	0:LB	0:PC	0:PC	O:PC	0:PC	PHA	PHA	PHA	PHA		H'A	PHA	PHA	H 1			AIS OTE	SIV
KEY No.				3910	3710	2710	2510	4310		2420	2730	2810	4260	4710	1940	2060		2085	0810	1230	2090	2720	1010	1120	1950			3310	4270	07/4	1210		0101	0 6 6	0661

